DECEMBER, 1950 25 CENTS

PF REPORTER

including Electronic Servicing

Regeneration in Picture-Signal Circuits

Report on TV Radiation Hazards

Examining Motorized Tuner Mechanisms

Speed Problems With Phonos

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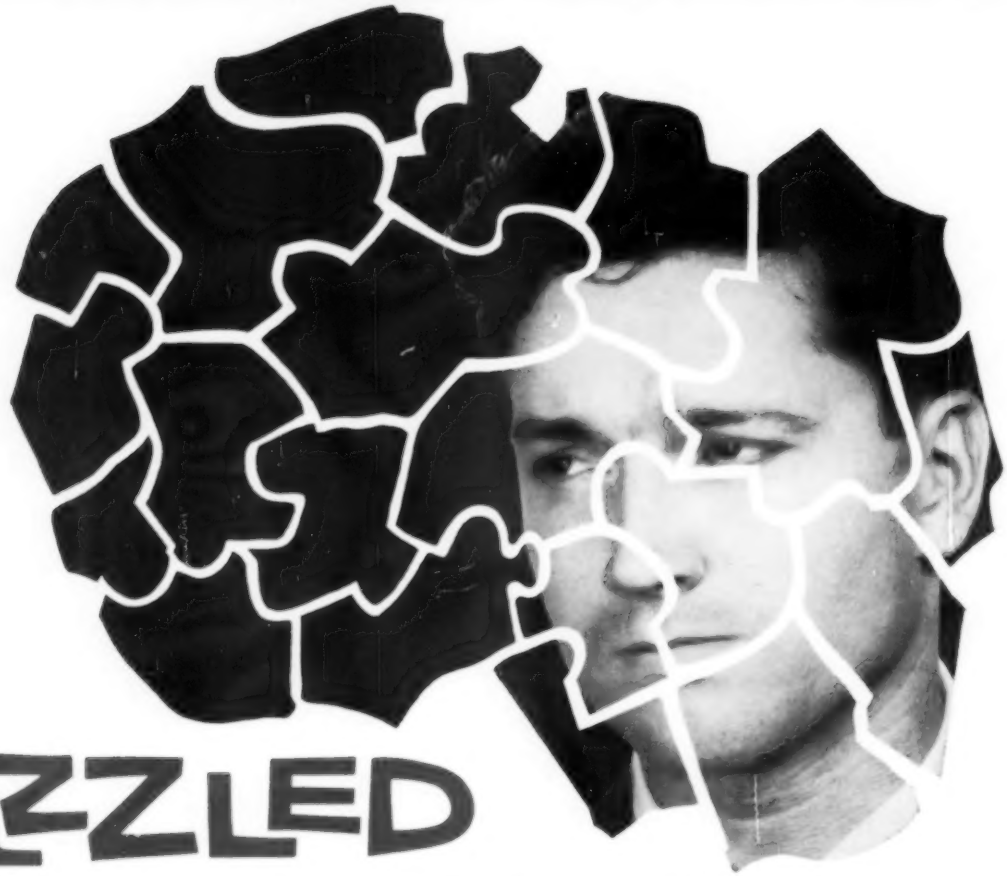

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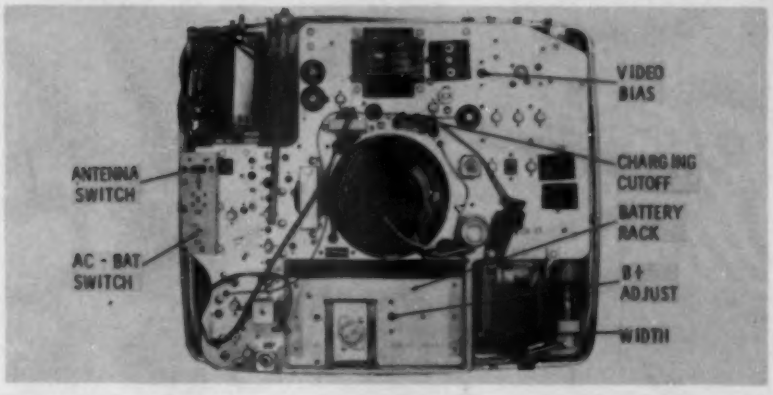
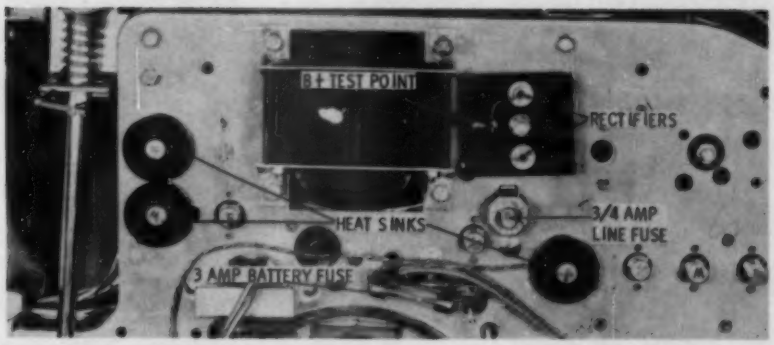
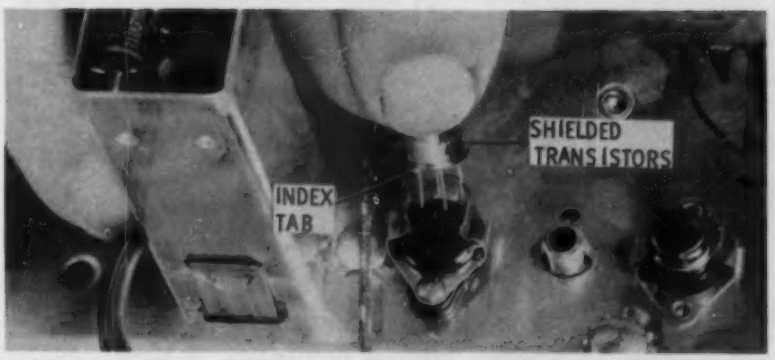
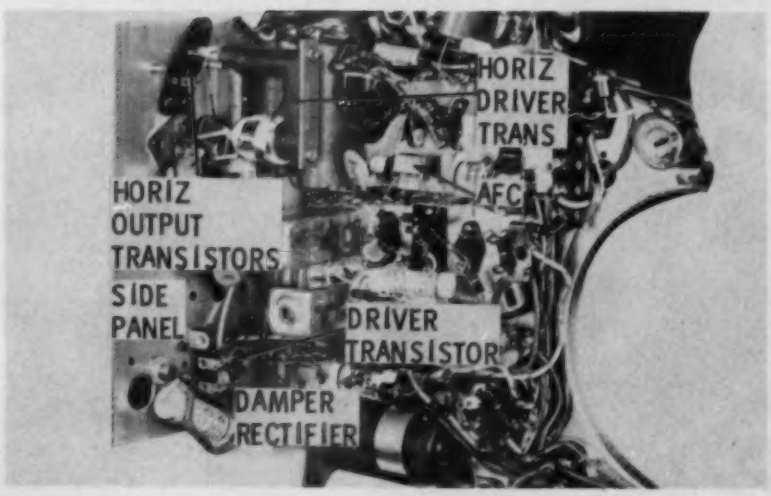
Motorola









Motorola Model 19P1 Chassis TS-432

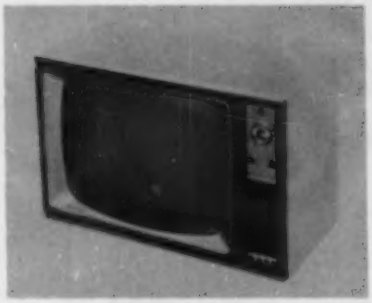
One of the outstanding models in Motorola's 1961 line is this 19" *Astronaut* transistorized portable. The 114° CRT used in this set (a 19AEP4) has a special filament rating of 12.5 volts, 150 ma. All operational controls are top-mounted, the channel selector and fine tuning knobs tilting forward for easier viewing. Height and linearity adjustments are accessible through the hollow shafts of the vertical and horizontal hold controls.

Removal of the cabinet exposes the clean-looking vertical chassis. The earliest versions were equipped with 23 transistors; however, horizontal output and B+ filtering circuits were changed to increase the number to 25. Several "never-before-heard-of" controls are employed in biasing and regulating circuits; consult the service data before attempting to make any setup adjustments. Two adjustments, AGC and vertical bias, are accessible through two holes in the bottom of the cabinet—these controls are hidden in the photo by the battery rack. The 1S2A high voltage rectifier is the only tube in the set other than the CRT. NOTE: High voltage should be checked with a meter; arcing the anode lead to chassis may damage the horizontal output transistors.

A full-wave silicon-rectifier power supply, used during AC operation, also charges the battery for portable operation. This circuit uses transistors as filters and voltage regulators, and its output should be adjusted to provide 19.5 volts at the test point with the set connected to a 122-volt AC source. Both the AC and battery supplies are fused. The heat sinks shown in the photo merely slide onto the transistor cases; be sure they are in place before operating the set.

Most of the transistors are plug-in units. Several sockets have four openings and are wired to ground the transistor shield through a fourth pin. An index tab or paint dot is provided on both three-and four-pin transistors to indicate how the transistor is to be inserted in the socket. When removing a transistor, make a special point to note the position of this tab or dot, since there are no mechanical stops to prevent you from incorrectly reinserting the unit.

The horizontal deflection circuits are mounted on a side panel that doubles as a heat sink. Since some of the sweep transistor and diode mountings are different from those you are accustomed to, we've pointed them out to help you find your way around.



RCA Victor
Model 231-BE-627
Chassis KCS132ZH

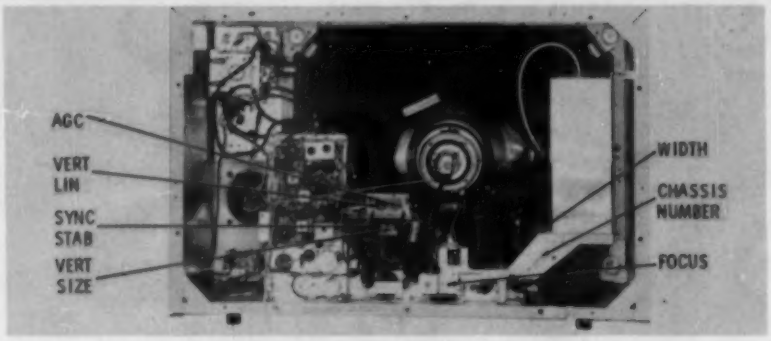
You'll do well to read this preview carefully, for it is applicable to 121 models and 33 chassis variations in RCA's 1961 line, and you're almost sure to encounter one of these sets. The vast majority of the models use the 23EP4, 110° tube with bonded safety shield like this set, but models equipped with the KCS131-series chassis use a 21DSP4 —a 90° tube. The *New Vista* emblem attached to this set is reserved for chassis containing the *Nuvistor*-equipped tuner. Other variations include UHF provisions, two different versions of remote control, and AM-FM-stereo additions.

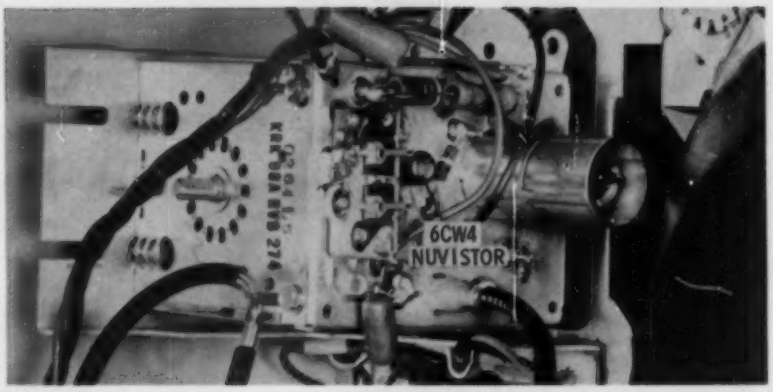
The general layout of the chassis is roughly "U" shaped, conforming quite closely with some previous designs. Most of the circuitry is contained on the two printed boards at the left—except the horizontal output stage and low-voltage supply, which are conventionally-wired. All setup controls are easily accessible, once the rear cover is removed.

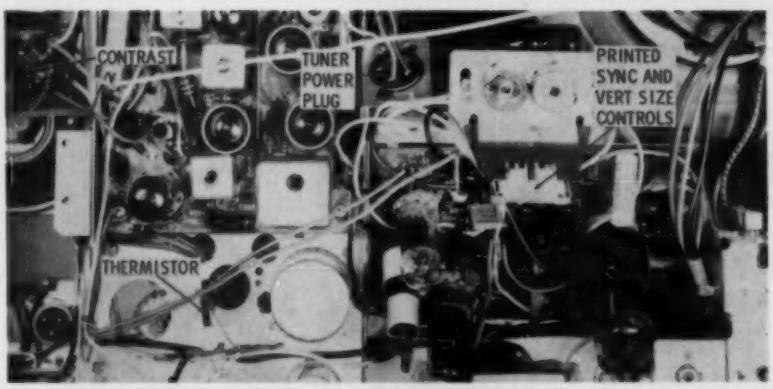
As mentioned, this chassis contains RCA's *Nuvistor*-equipped tuner — a marked departure in tuner design and tube basing. (For a full account of this tuner, see "Advances in TV Tuners" in the September issue of PF REPORTER.) Other versions of the chassis use either a turret tuner or a standard RCA incremental-switch type.

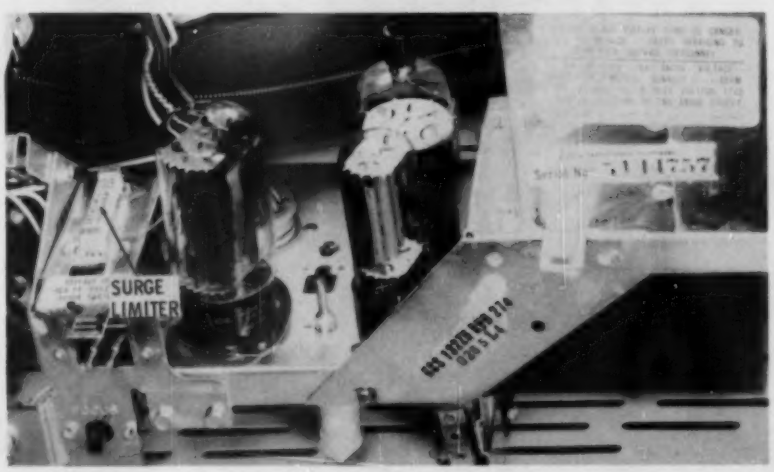
The printed-wiring detail follows the same pattern established in earlier RCA receivers. The contrast control is mounted in a rather unusual manner, and is connected by two couplings to the knob on the front. Power for the tuner is provided through a plug-and-socket arrangement at a junction of the printed boards. The *thermistor* at the lower left is connected in series with the AC line to provide controlled tube warm-up; it's rated at 120 ohms cold. A printed component combination including the sync and vertical size controls also contains two printed resistors associated with the sync circuits, as does its three-control counterpart used in some other chassis this year.

Most of the circuit variations between the KCS131 and 132 series are centered in the horizontal deflection circuits, so be sure you're following the correct service data when confronted with trouble in this section. Consistent with RCA's policy of previous years, the fusible resistor is defined as a surge limiter and rated at 3/10 amp. (It's connected to provide sweep-circuit protection.) Two lengths of #28 wire, located beneath the chassis, are used for filament protection.

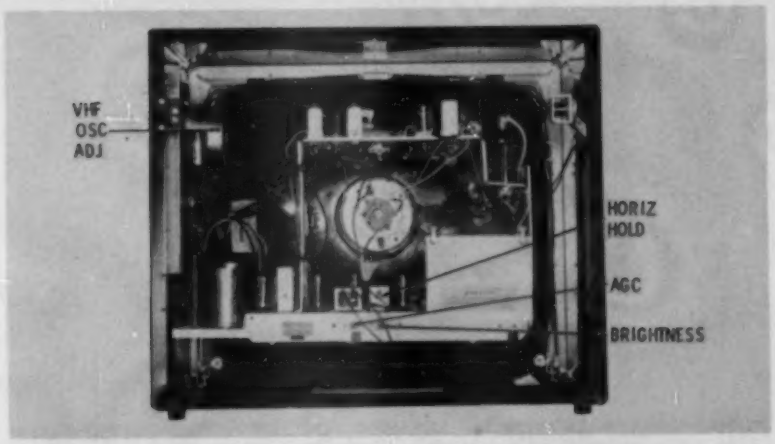








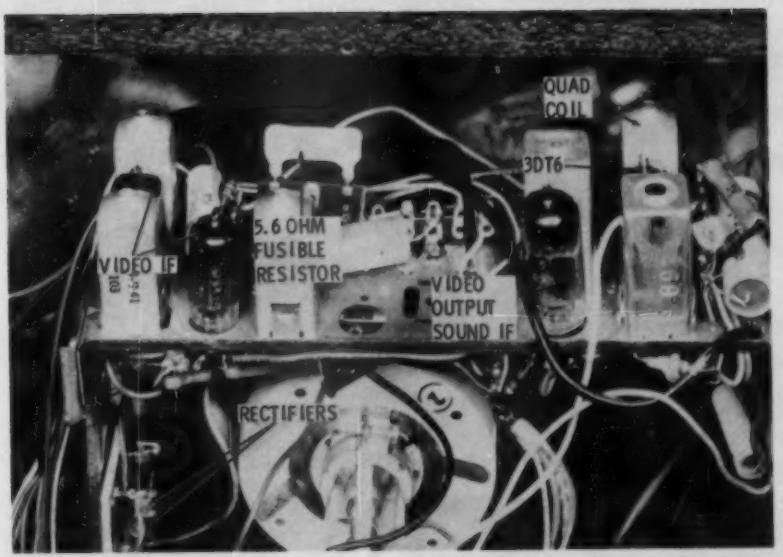
Trav-Ler



Trav-Ler Model 23MT6055
Chassis 1150-80

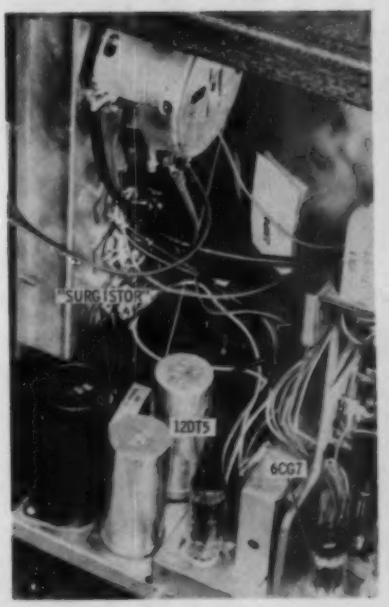
This early 1961 Trav-Ler table model is equipped with a 23GP4 CRT with bonded safety shield. Two very similar chassis, the 1150-89 and 1156-89, use a 17DTP4. All are 110° versions with only minor electrical variations. Side-mounted controls are common to all the models, and provide channel selection, on-off-volume, contrast, and vertical hold. The last two have hollow shafts for access to the vertical linearity and height adjustments.

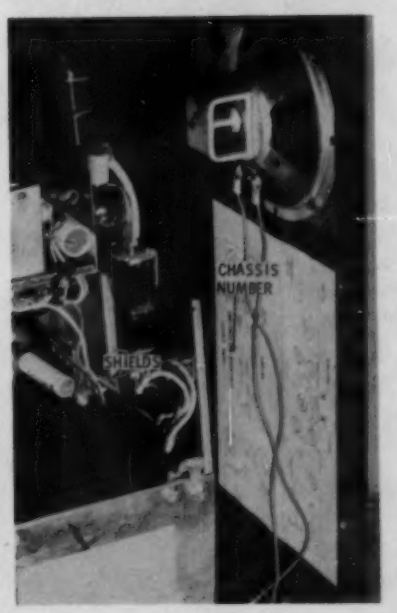
Following the same general layout of one of its 1960 predecessors, the 15-tube chassis is one of the last series-filament versions of the Trav-Ler line. (All later designs use power transformers.) As in its '60 counterpart, a *Fireball* tuner is used, making the VHF oscillator adjustments accessible from the rear of the set. The AGC control of this chassis serves as an adjustable grid-load resistor which varies the amplitude of the input signal fed to the grid of the 3BU8 keyer. All of the rear-mounted controls are fitted with phenolic tubing which protrudes through the rear cover to permit adjustment and still maintain isolation from the "hot" chassis.



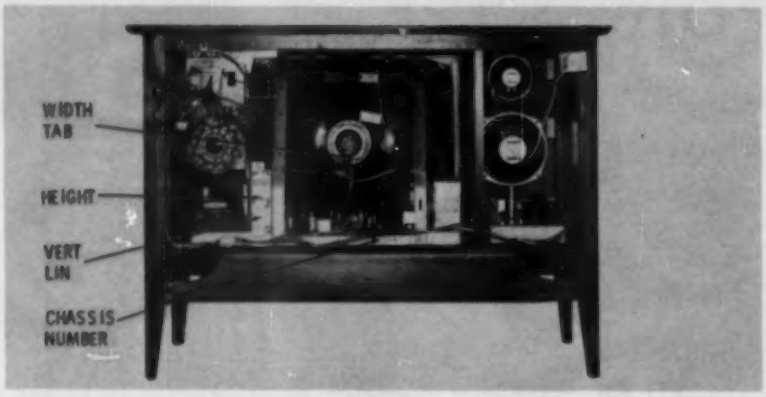
The top shelf of the chassis is divided sharply between the two-stage video IF section to the left, and the video output, sound IF, and 3DT6 audio detector circuits to the right. The pair of silicon rectifiers serving the conventional half-wave voltage-doubler circuit are directly below the shelf on the vertical chassis support, while the 5.6-ohm fusible resistor protecting them plugs into a board mounted on the shelf.

The left end of the base chassis contains the combined vertical multivibrator and output circuit, which uses one section of a 6CG7 and a 12DT5. The other 6CG7 section serves in a sync phase inverter circuit. On the extreme left of the subchassis, the 1150-89 chassis used in one of the 17" versions uses two different electrolytic filters and omits the *surgistor*. The latter is a thermal switch that protects tube filaments during warm-up.





The chassis used in any Trav-Ler model can be identified by referring to the number printed on the tube layout chart glued to the side of the cabinet. Above the high-voltage cage, the horizontal output and damper stages are mounted on a subchassis equipped with shields to keep the heat away from the remaining circuits.



Westinghouse
Model H-K4410
Chassis V-2389-3

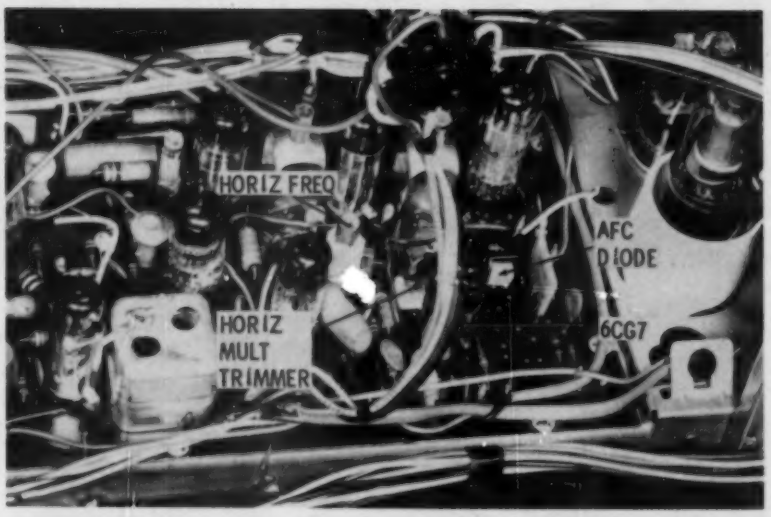
Using the largest chassis in the 1961 Westinghouse line, this 23", 114° model has a conventional safety glass secured by three wood screws and a trim strip along the top edge. VHF, UHF-VHF, and remote-control versions are designated by -1, -2, and -3 numbers associated with the basic V-2389 chassis number.

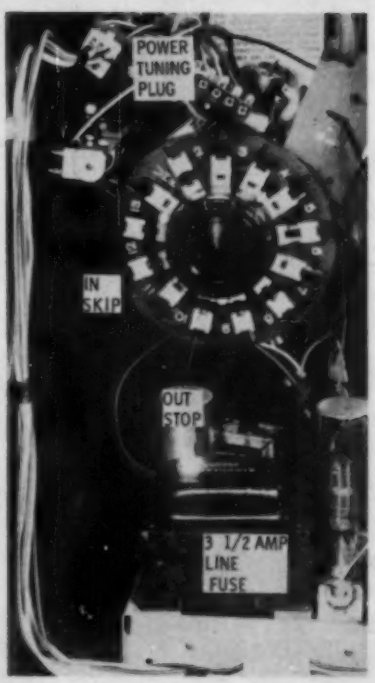
The horizontal chassis, characterized by two large, curved rails holding the CRT, has surprisingly great width. Two conventionally-wired end sections contain the power supply and horizontal output circuits, while one large printed board, containing the rest of the circuitry, fills the area between them. Height and vertical-linearity adjustments are the only rear-mounted controls on this 18-tube chassis. A new adaptation of the conventional width sleeve, in the form of a piece of copper bonded into a phenolic tab, is inserted between the yoke and bottom side of the CRT neck. It's held in place by the yoke clamp, and *must* retain its position along the bottom of the neck.

The bottom side of the printed board contains the *See-Matic* identification system introduced by Westinghouse in their 1960 models. The horizontal frequency and multivibrator trimmer adjustments are directly below the CRT neck, just in front of the partially shielded 6CG7 multivibrator.

In models equipped with power tuning, plastic bars above and below the nameplate provide bidirectional channel selection. Bass and treble switches are positioned at the bottom of the control panel, next to the *memory tuning* knob — a "do-it-yourself" fine tuning adjustment. The PULL-ON REMOTE switch at the top works in conjunction with the regular off-on switch to turn on the 7-tube remote receiver — a supersonic unit controlled by transistor-generated signals.

A 3½-amp. type-N line fuse protects the power transformer, which has a 12-volt center-tapped secondary for filament power. The center tap is grounded, providing two 6-volt legs (each with its own fuse wire). Three 12-volt tubes are used in the chassis—a 12AX4GTB, 12DT5, and 12DQ6B. These are connected in parallel across the entire 12-volt winding. A plug-in cable coming from the power supply feeds power to the tuning unit. These 1961 models have the same programming adjustments as for '60. With the cam for a certain channel pushed in, the tuner skips that channel; leaving the cam in the outer position stops the tuner.





See PHOTOFACT Set 483, Folder 1

See PHOTOFACT Set 483, Folder 1

Mfr: General Electric **Chassis No. U4**

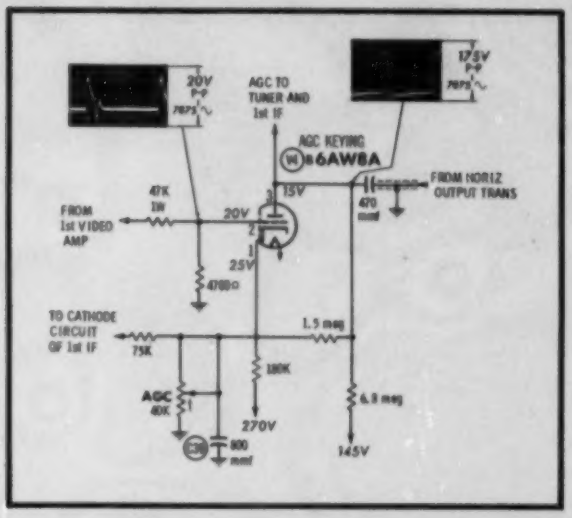
Card No: GE U4-7.

Section Affected: Pix and sound.

Symptoms: Loss of both picture and sound.

Cause: Video overloading as a result of shorted AGC cathode-bypass capacitor.

What To Do: Replace C39 (800 mmf).



Mfr: General Electric **Chassis No. U4**

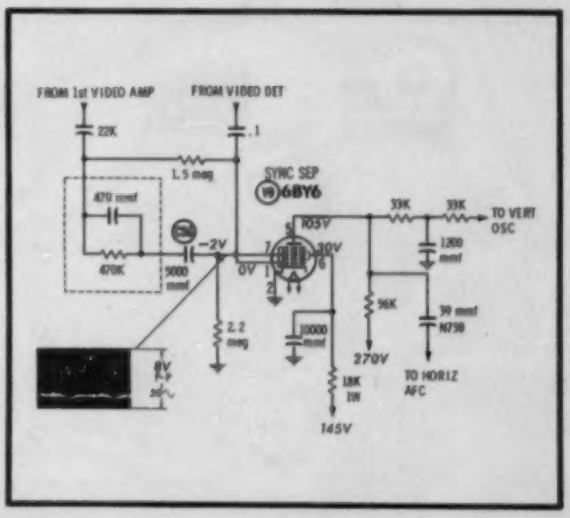
Card No: GE U4-8

Section Affected: Sync; possibly also sound.

Symptoms: Unstable sync; horizontal phase shift; possible audio buzz. Positive voltage on control grid (pin 7) of 6BY6 sync separator.

Cause: Leaky or shorted capacitor in sync-separator grid circuit.

What To Do: Replace C56 (5000 mmf).



Mfr: General Electric **Chassis No. U4**

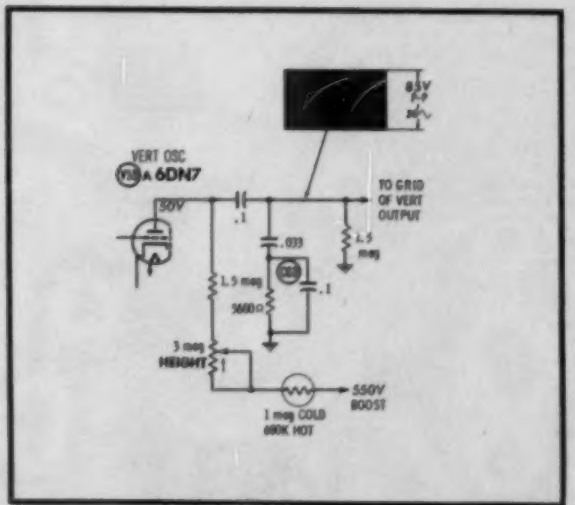
Card No: GE U4-9

Section Affected: Sync and raster.

Symptoms: Insufficient height and poor vertical sync.

Cause: Open capacitor in vertical sawtooth-forming network.

What To Do: Replace C63 (.1 mfd).



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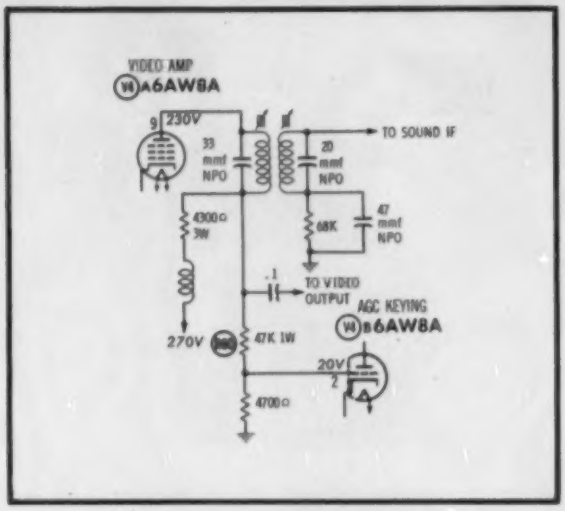
See PHOTOFACT Set 483, Folder 1



See PHOTOFACT Set 483, Folder 1

Mfr: General Electric **Chassis No. U4**

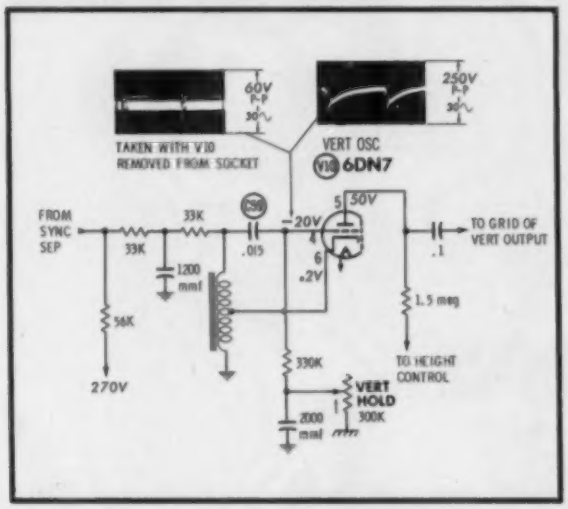
Card No: GE U4-10

Section Affected: Pix and sound.

Symptoms: No pix; buzz in sound; incorrect grid voltage on AGC keying tube.

Cause: Increase in value of series resistor between plate of video amplifier and grid of AGC tube.

What To Do: Replace R60 (47K—1W).



Mfr: General Electric **Chassis No. U4**

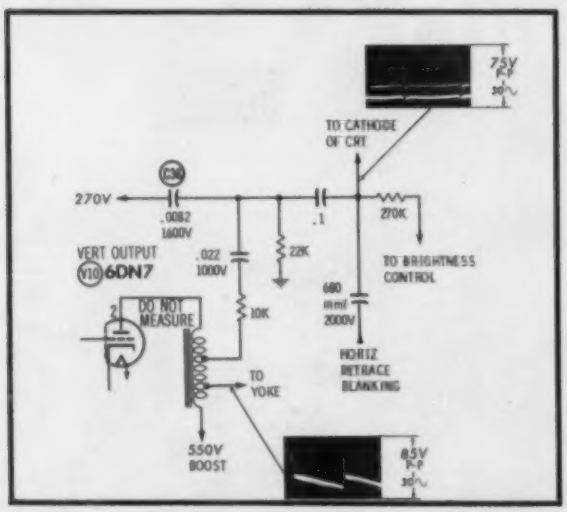
Card No: GE U4-11

Section Affected: Raster and sync.

Symptoms: Vertical foldover at top; unstable vertical sync. Positive or only slightly negative voltage at grid (pin 4) of V10, vertical oscillator.

Cause: Leaky vertical-oscillator grid capacitor.

What To Do: Replace C59 (.015 mfd).



Mfr: General Electric **Chassis No. U4**

Card No: GE U4-12

Section Affected: Raster.

Symptoms: Dim raster with dark shading on right.

Cause: Open vertical retrace-blanking capacitor.

What To Do: Replace C36 (.0082 mfd — 1600V, 10%).

See PHOTOFACT Set 491, Folder 2

See PHOTOFACT Set 491, Folder 2

Mfr: Zenith **Chassis No. 18E20**

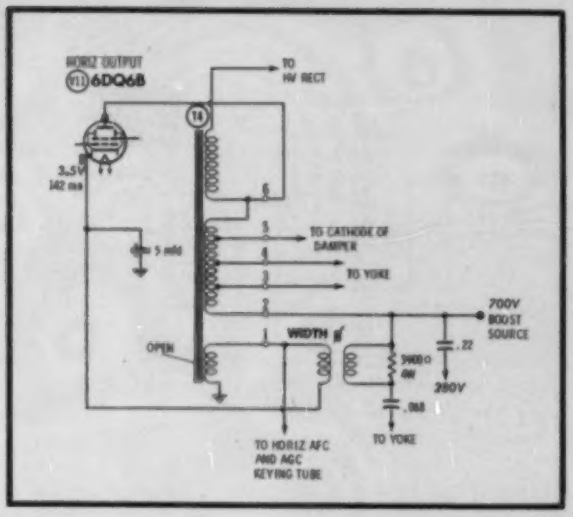
Card No: ZE 18E20-1

Section Affected: Raster.

Symptoms: No raster; no high voltage.

Cause: Open cathode winding on horizontal output transformer.

What To Do: Replace T4.



Mfr: Zenith **Chassis No. 18E20**

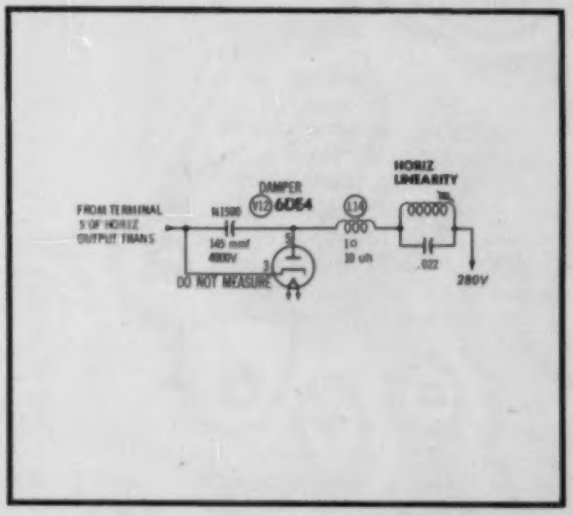
Card No: ZE 18E20-2

Section Affected: Raster.

Symptoms: Raster flashes on and off.

Cause: Intermittently open RF choke at plate of damper.

What To Do: Replace L14.



Mfr: Zenith **Chassis No. 18E20**

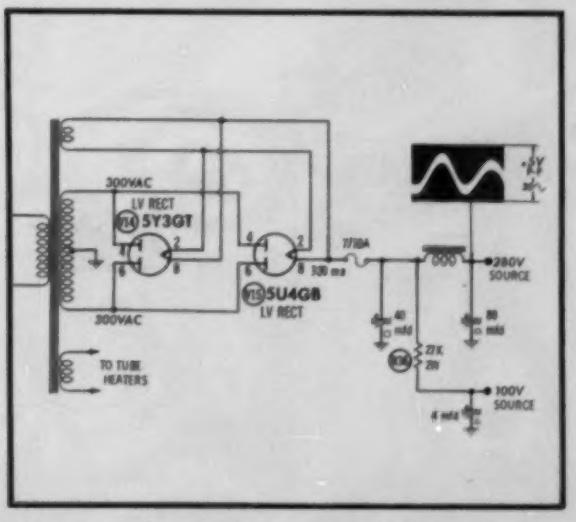
Card No: ZE 18E20-3

Section Affected: Pix.

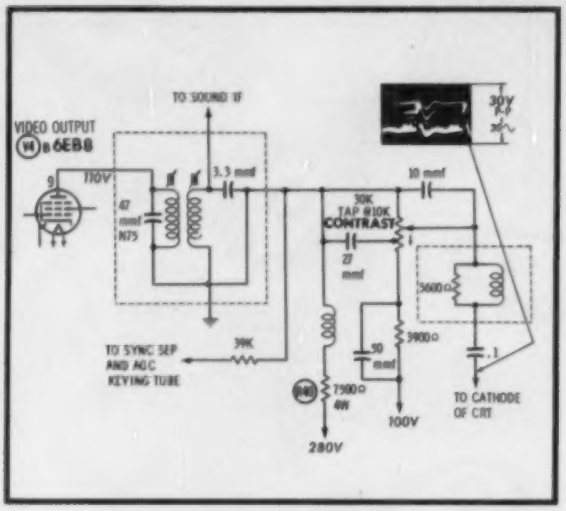
Symptoms: Video disappears about one-half hour after set is turned on.

Cause: Open series resistor in 100-volt (low B+) line.

What To Do: Replace R36 (27K—2W).



See PHOTOFACT Set 491, Folder 2



See PHOTOFACT Set 491, Folder 2

Mfr: Zenith **Chassis No. 18E20**

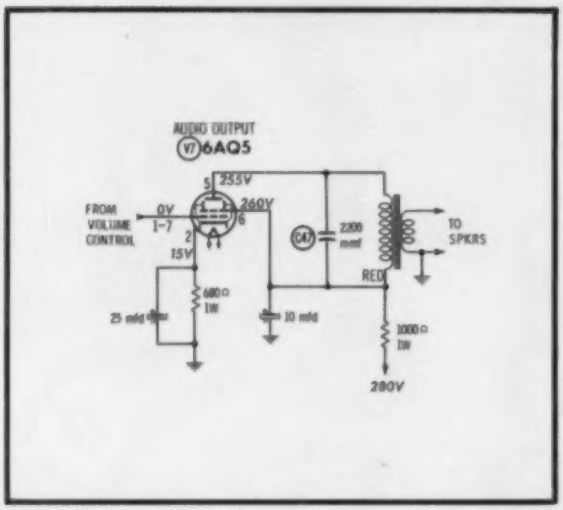
Card No: ZE 18E20-4

Section Affected: Pix.

Symptoms: Picture weak and smeared.

Cause: Plate-load resistor in video output stage has decreased in value.

What To Do: Replace R40 (7500 ohms—4W).



Mfr: Zenith **Chassis No. 18E20**

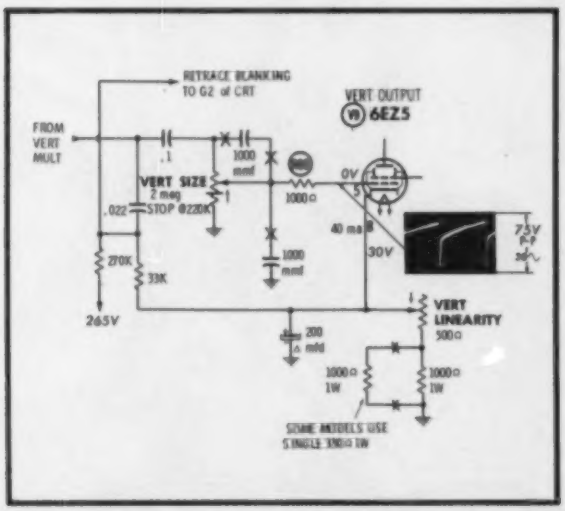
Card No: ZE 18E20-5

Section Affected: Sound.

Symptoms: No sound.

Cause: Shorted plate-bypass capacitor in audio output stage.

What To Do: Replace C47 (2200 mmf).



Mfr: Zenith **Chassis No. 18E20**

Card No: ZE 18E20-6

Section Affected: Raster.

Symptoms: Intermittent vertical collapse.

Cause: Defective series resistor in grid circuit of vertical output tube.

What To Do: Replace R69 (1000 ohms); also check V9 (6EZ5).

SYLVANIA-6AU4-GTA

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"WRAP-UP" PROFITS!

NEW life-giving, profit-building features are built into every SYLVANIA-6AU4-GTA TV-damper tube. Consider, for one feature, the SYLVANIA SARONG CATHODE and how it adds dependability to tube life. SARONG provides uniform spacing between cathode and plate—reduces possibility of plate-to-cathode arc-over. SARONG prevents the build-up of "whiskers" inside the cathode sleeve that can develop during other types of coating processes—reduces possibilities of cathode-to-heater arc-over.

Consider, too, the "pigtail" heater in SYLVANIA-6AU4-GTA. Welded securely to the stem-lead, it reduces heater "hot spots" and the possibilities of heater burnout. More . . . rectangular top and bottom micas with exceptionally wide slots increase the resistance of dc leakage paths, further reduce the possibilities of internal arc-over and breakdown.

There's extra profit assurance, too, with SYLVANIA-6AU4-GTA. Every one of them is tested for shorts, emission and the ability to withstand arc-over at 5000-volts peak inverse on the anode.

So, "wrap up" the profits you make by putting a "damper" on call-backs. When you ask your distributor for 6AU4-GTA's, always specify SYLVANIA.

Electronic Tubes Division, Sylvania Electric Products Inc., 1740 Broadway, New York 19, New York.

SYLVANIA

Subsidiary of **GENERAL TELEPHONE & ELECTRONICS**

Another outstanding product by the HIDDEN 500* who plan for your future:

TYPE TE
LITTL-LYTIC® CAPACITORS

Transistors revolutionized the industry. And to make the most of their inherent advantages, they called for an entirely new group of components. Here, Sprague Research was the first to answer the call with the smallest truly reliable dry electrolytic made for transistor circuits —the Littl-Lytic. This reasonably priced capacitor is the most reliable subminiature you can buy for transistorized radios, hearing aids, wireless microphones, pocket wire recorders, and other miniature electronic equipment.

The remarkable reliability of Littl-Lytic is the result of a new manufacturing technique in which *all the terminal connections are welded.* Units are hermetically sealed and metal encased . . . *with no pressure joints* . . . there are *no "open circuits" with the passage of time.* Leakage current is extremely low as the result of the use of high purity foil and ultra-stable formation techniques. Sprague's catalog replacement ratings are the most comprehensive in the industry. They assure you of exact replacements to meet your day-to-day service requirements.

Littl-Lytic is a typical example of how Sprague Research keeps its products up-to-the-minute. Reliable components mean reliable service work—your business keeps pace with the electronic industry when you use Sprague.

***The "Hidden 500"** are Sprague's 500 experienced researchers who staff the **largest research organization in the electronic component industry** and who back up the efforts of some 6,000 Sprague employees working in 14 manufacturing operations—four at North Adams, Mass.; Bennington and Barre, Vt.; Concord and Nashua, N.H.; Lansing, N.C.; Grafton, Wis.; Visalia, Calif.; two at Ponce, Puerto Rico; and Milan, Italy.

don't be vague . . . insist on **SPRAGUE®**

world's largest capacitor manufacturer

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PF REPORTER

including Electronic Servicing

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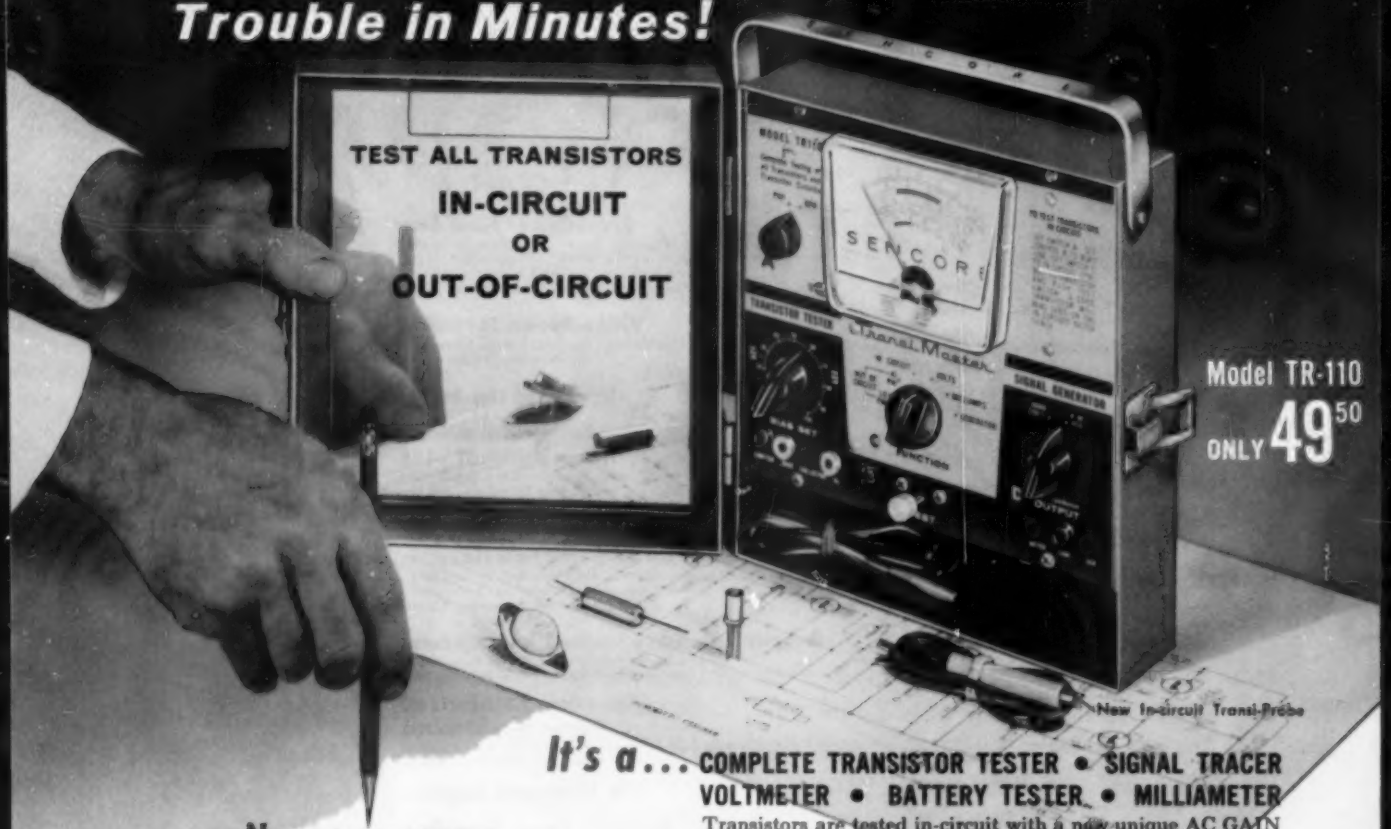
ABOUT THE COVER

It isn't Macy's, but then you don't have to have a fancy address for a window display to be worthwhile. With a little thought and ingenuity, you can come up with a "do-it-yourself" display that will do wonders for your Christmas business. Time is short, but there's still a couple of weeks left to attract last-minute shoppers. While we're on the subject of Christmas, a very merry one to you and yours from the entire staff.

NEW SENCORE Transi Master

Analyze Every Transistor Circuit Trouble in Minutes!



Model TR-110
ONLY 49.50

New In-circuit Transi-Probe

It's a... COMPLETE TRANSISTOR TESTER • SIGNAL TRACER VOLTMETER • BATTERY TESTER • MILLIAMETER

Transistors are tested in-circuit with a new unique AC GAIN check and out of circuit with an accurate DC GAIN and LEAKAGE check. Set-up chart included for reference only.

Now you can . . .

- **Test all transistors in-circuit** with a new unique AC GAIN check. It works every time and without the use of the set-up booklet.
- **Test all transistors out of circuit** with the AC GAIN check or with a more accurate DC current gain and leakage check.
- **Read current gain (beta) direct** for experimental, engineering work or for matching transistors.
- **Check diodes** simply and accurately with a forward to backward ratio check.
- **Signal trace** from speaker to antenna with a special low impedance generator. No tuning, adjustments, or indicating device needed for transistor radio trouble shooting. Just touch output leads to transistor inputs and outputs until 2000 cycle note is no longer heard from speaker. (Generator output monitored by meter.) It's a harmonic generator for RF-IF trouble shooting and a sine wave generator for audio amplifier trouble shooting.
- **Check batteries** under operating conditions as well as the voltage dividers with a special 12 volt scale.
- **Monitor current** drawn by the entire transistor circuit or by individual stages with a 0 to 50 Ma current scale. A must for alignment and trouble shooting cracked boards.

Benefit from these Sencore extras

- Lists Japanese equivalents.
- Automatically determines NPN or PNP.
- Mirror in detachable cover to reflect opposite side of printed board.
- Special clip to fit between batteries for current check.
- Transi-probe for making in-circuit transistor checks.

Color	modern two tone gray
Size	8" x 7¼" x 3"
Weight	only 5 lbs.
Meter	0 to 3 Ma, 3½", 5% tolerance, modern plastic
Batteries	two size "C" cells

ALL PARTS ARE [illegible] MADE IN AMERICA

SENCORE

ADDISON, ILLINOIS

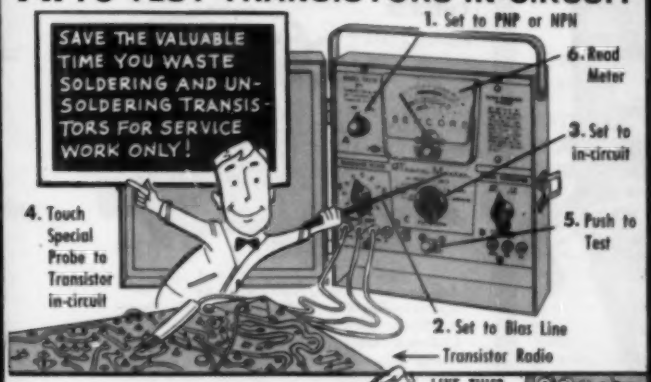
Like to try it? Let Sencore Sam show you how and then see your Sencore Distributor. He has it in stock. . .

SENCORE SAM

THE MINIT-MAN

SHOWS YOU HOW TO USE THE
SENCORE TRANSI-MASTER

A. TO TEST TRANSISTORS IN-CIRCUIT

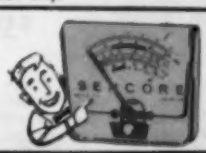

SAVE THE VALUABLE TIME YOU WASTE SOLDERING AND UN-SOLDERING TRANSISTORS FOR SERVICE WORK ONLY!
1. Set to PNP or NPN
6. Read Meter
3. Set to in-circuit
4. Touch Special Probe to Transistor in-circuit
5. Push to Test
2. Set to Bias Line
Transistor Radio

The in-circuit check can also be used for a quick check on transistors out of circuit.

B. TO TEST TRANSISTORS OUT OF CIRCUIT FOR GAIN, LEAKAGE, OPENS, SHORTS

USE THIS DC CHECK FOR MOST ACCURATE TEST. USE SET-UP BOOKLET.
1. Determine Transistor Type. Set-up according to book
5. Normal Transistor will be in Green area of Gain Scale
3. Read Leakage and Compare to Chart
2. Connect to transistor. Use 4th leader for tetrode only.
4. Push to test Gain

Want to read Beta direct? Just set Bias Control to bias line and read meter. It's handy for engineers and when matching transistors.



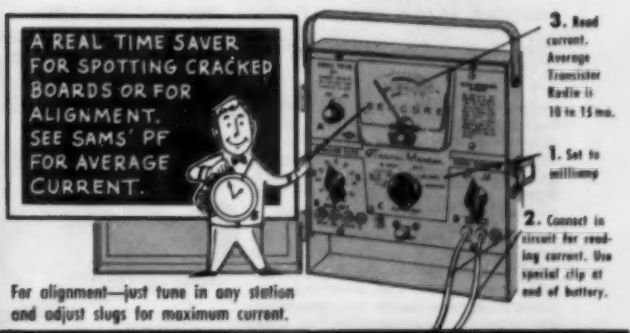
For matching . . . pick the two transistors with closest Beta reading. The two transistors should also have approximately same leakage.

C. TO SIGNAL TRACE TRANSISTOR CIRCUIT

YOU CAN FIND THE DEFECT IN A JIFFY!
1. Set Switch to Generator
3. Meter will indicate when generator is putting out
2. Set according to stage
5. Touch to transistor inputs and outputs from speaker to antenna. 2000 cycle note from speaker will stop or decrease at trouble spot.
4. Connect to common or ground
TRANSISTOR RADIO

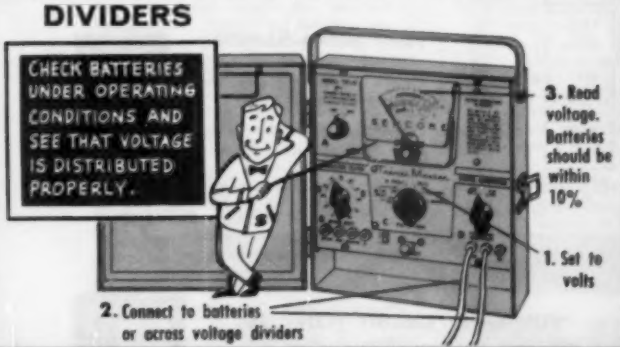
D. TO CHECK CURRENT DRAIN

BY COMPLETE SET OR INDIVIDUAL STAGE

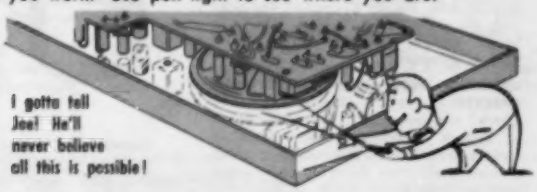

A REAL TIME SAVER FOR SPOTTING CRACKED BOARDS OR FOR ALIGNMENT. SEE SAMS' PF FOR AVERAGE CURRENT.
3. Read current. Average Transistor Radio is 10 to 15 ma.
1. Set to milliamp
2. Connect in circuit for reading current. Use special clip at end of battery.

For alignment—just tune in any station and adjust slugs for maximum current.

E. TO CHECK BATTERIES AND VOLTAGE DIVIDERS


CHECK BATTERIES UNDER OPERATING CONDITIONS AND SEE THAT VOLTAGE IS DISTRIBUTED PROPERLY.
3. Read voltage. Batteries should be within 10%
1. Set to volts
2. Connect to batteries or across voltage dividers

AND LAST OF ALL . . . the mirror in the detachable cover. Just place it under the printed board to see the other side as you work. Use pen light to see where you are.



ALSO FREE . . . Current transistor listings booklet, even has Japanese equivalents . . . just send in your warranty card and factory will keep you up to date!

Ask your distributor to show you the most useful equipment in servicing —

SENCORE

Transi Master
by SENCORE
ADDISON, ILLINOIS

SENCORE

Most Popular Time Savers for Servicemen, Technicians, Engineers, Maintenance Men, Hobbyists!

"MIGHTY MITE"

TUBE CHECKER

Smaller than a portable typewriter . . . yet will outperform testers costing hundreds of dollars.

$59.50

A new dynamic approach to tube testing. Check over 1,300 tubes for cathode emission, grid emission, leakage, shorts and gas. A "mite" to carry but a whale of a performer that outperforms testers costing much more. New unique "stethescope" approach tests for grid emission and leakage as high as 100 megohms yet checks cathode current at operating levels. Special short test checks for shorts between all elements. The Mighty Mite will test every radio and TV tube that you encounter (over 1,300!) plus picture tubes. Set up controls as easy as "ABC" from easy to follow tube chart. New features: • Meter glows in dark for easy reading behind TV set. • Stainless steel mirror in cover for TV adjustments. • Rugged, all steel carrying case and easy grip handle. • Smallest complete tester made. Measures only 9" x 8" x 2½" and weighs just seven pounds.

It's a real money-maker

LC3 LEAKAGE CHECKER

Provides grid emission and leakage checks with the same sensitivity as the famous Mighty Mite but checks critical tubes only; 172 types

$28.95

Ask any serviceman who owns one . . . or try one for just one day of servicing. You'll see for yourself how much time the LC3 can save you. Checks for leakage between all elements, whether caused by gas, grid emission or foreign particles. Also checks leakage on all capacitors with voltage applied — including electrolytics. Provides instant filament checks in "Fil-Check" position—no need for a second filament checker. One spare pre-heating socket and new roll chart prevent obsolescence. New charts provided free. For 110-120 volts, 60 cycle AC.

SENCORE SS105 SWEEP CIRCUIT TROUBLE SHOOTER

The Missing Link in TV Service . . .

$42.95

IT'S A . . .

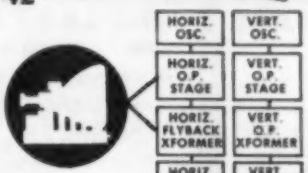
UNIVERSAL HORIZONTAL OSCILLATOR. For direct substitution. No wires to disconnect in most cases. Traces trouble right down to the defective component. Variable output from 0-200 volts, peak-to-peak. Oscillator will sync to TV sync signal giving check on sync circuits.

HORIZONTAL OUTPUT CATHODE CURRENT CHECKER. A proven method that quickly checks the condition of the horizontal output tube and associated components. Adaptor socket prevents breaking wires. Easily replaceable Roll Chart gives all necessary pin, current and voltage data. New Roll Charts are Free.

UNIVERSAL DEFLECTION YOKE. A new, simple way to determine yoke failure accurately—without removing yoke from picture tube. Merely disconnect one yoke lead and substitute. If high voltage (also bright vertical line) is restored, TV yoke is defective.

DYNAMIC FLYBACK TRANSFORMER CHECKER. Merely flip switch to "Flyback Check" and meter will indicate condition of flyback transformer, in degrees of horizontal deflection. Extremely sensitive and accurate; even shows up one shorted turn on flyback.

VOLTMETER. For testing bootstrap, screen and other voltages. Direct-reading voltmeter, 0-1000 volts.



UNIVERSAL VERTICAL OSCILLATOR. Checks oscillator, output transformer and yoke. Merely touch lead to component and check picture on screen.

SS105 is completely self-contained, nothing else is needed.

New, improved Circuit.

FC4 FILAMENT CHECKER

The ideal tool for servicing series string filaments.

$2.75

Purposely works off your cheater cord to give you a positive check on line voltage. Prevents checking all tubes to find that your trouble was no line voltage. Only checker that checks all tubes automatically and has no batteries to replace. Cost half that of battery operated testers. Patented.

FC4 with test leads for checking continuity or AC or DC Voltage **$2.95**

VB2 "VIBRA-DAPTOR"

Checks 3 and 4 prong Vibrators Faster and Easier . .

Plugs into any tube checker; ideal for use with LC3 or the Mighty Mite. To check 6v. vibrators, set for 6AX4 or 6SN7; for 12 v. vibrators, set for 12AX4 or 12SN7. Two No. 51 lamps indicate whether vibrator needs replacing. Instructions on front panel. Steel case.

$2.75

"FUSE-SAFE" CIRCUIT TESTER FS3

Instantly tells you whether or not it is safe to replace fuse resistors, fuses, or circuit breakers. Separate red and green scale for each commercially available fuse resistor used in radio and TV. Eliminates guesswork, wasted time. Also handy for wattage checks up to 1100 watts at 115v.

$8.95

Time Savers for America's **Radio, TV** *and Electronic Minit-Men*

ALL PARTS MADE IN AMERICA

See your Parts Distributor Now or Mail Coupon on Opposite Page

SENCORE

You can own all these popular Time Savers for less than some Mutual Conductance Tube Testers!

For TRANSISTOR RADIO SERVICING

Everything you need for less than $50.00

SENCORE TRC4

TRANSISTOR-RECTIFIER CHECKER

$19.95

Now lists Japanese equivalents

Checks Transistors, Diodes, Rectifiers . . . A transistor tester that is used by over 50,000 servicemen, engineers and experimenters from Coast to Coast. Recommended by TV and Radio manufacturers; used by such leading companies as Sears Roebuck, Bell Telephone and Commonwealth Edison. Tests indicate that the TRC4 will outperform testers costing many times more. The TRC4 tests all transistors for gain, leakage, and open or shorts. Simple to operate without set-up chart for service work and with set-up chart for more accurate checks. With batteries.

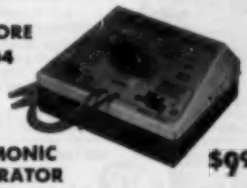
SENCORE PS103

BATTERY ELIMINATOR & TROUBLE SHOOTER

$19.95

Replaces Batteries During Repair . . . Replaces batteries during repair time of transistor radios and helps trouble shoot, too. For transistor radio servicing, experimenting and to charge nickel cadmium batteries. Dial output voltage from 0 to 24 volts DC and read on meter. Low ripple insures no hum or feedback problem. Meter reads from 0 to 100 MA. Shorted stage will cause current to read high as indicated on PF schematics; open stage will cause current to read low. To align transistor radio, tune in station signal and adjust IF slugs for maximum current. The PS103 is the only supply that will operate radios with tapped battery supplies; such as Philco, Sylvania, Motorola, etc.

SENCORE HG104



HARMONIC GENERATOR

$9.95

Finds Defective Stage in a Minute . . . Believe it or not. Just touch the output leads of the HG104 to inputs and outputs of transistors and a clear 1000 cycle note from speakers will tell you whether or not the stage is defective. Here is an unexcelled time saver, not a "pencil" gimmick. It actually works every time from speaker to antenna. Two leads and calibrated output (not found on pencils) are a must for speaker connection, grounding to prevent RF spray and front end checks. Also saves time when servicing HiFi, TV and radios. With life-time batteries.

Get all 3 ▶ **COMPLETE TRANSISTOR RADIO SERVICE LAB**

All 3 Time Savers shown above in handsome display carton carrying case

MODEL TL107

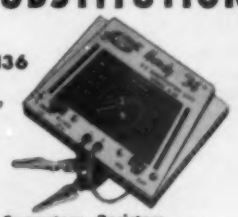
$49.85

For SUBSTITUTION SERVICING

Goodby to messy parts . . . the mess of soldering and unsoldering in testing.

SENCORE H36

"HANDY 36"



$12.75

Substitute for Capacitors, Resistors . . . Provides the 36 most often needed resistors and capacitors for experimenting, substituting or testing. Eliminates searching for replacement components, unnecessary soldering and unsoldering and the mess it creates. Says goodbye to crumpled parts. Flick of a switch instantly selects any of: 24 Resistors from 10 ohms to 5.6 megohms, 10 Capacitors from 100 mfd to .5 mfd, 2 Electrolytics, 10 mfd and 40 mfd at 450 Volts. All components are standard American brand.

SENCORE ES102

ELECTRO-SUB

$15.95

Substitute for Electrolytic Capacitors . . . Complete, safe substitution . . . from the smallest electrolytics used in transistor radios to the largest used in costly Hi-Fi amplifiers. Contains 10 electrolytics from 4 to 350 mfd. Select correct value with the flick of a switch. Features automatic discharge, surge protector circuit. Prevents accidental "healing" of capacitor being bridged. Completely safe—no arc or spark when connecting or disconnecting. Usable from 2 to 450 volts, DC.

SENCORE RS106

RECTIFIER TROUBLE-SHOOTER

$12.75

Locate faulty Rectifiers, Diodes . . . This unique substitution unit simplifies trouble shooting rectifiers and diodes, gives you a positive check every time. Substitute for suspected rectifier or diode, watch picture or listen to sound and you'll know in seconds whether or not the rectifier or diode should be replaced. No guess work, soldering mess or time lost. The RS106 costs less than having loose rectifiers and diodes in the shop for testing and is worth many times more. A must for servicing voltage doubler circuits. Protected by a ½ amp. Slow Blow Fuse.

All 3 Time Savers shown above in handsome display carton carrying case

MODEL SL108

$41.45

See your Distributor . . . if he cannot help you, Pat will! . . .

PAT RUDE, Customer Service

SENCORE BE3 "ALIGN-O-PAK"

Eliminates messy batteries in TV service work. Handy for alignment, AGC trouble-shooting or checking gated sync circuits. Dial the voltage you need, 0-18 volts, positive or negative. Completely isolated DC supply, less than 0.1% ripple. Covers all voltages recommended by TV set manufacturers and in Photo Fact schematics. For 110-120V, 60 cycle AC.

$78.95

SENCORE, ADDISON 4, ILLINOIS

Dear Pat: Will you please . . .

☐ Send me _____ Time Savers
(Model Numbers)

☐ Check or M.O. enclosed (PP Prepaid.) ☐ Send C.O.D.

Distributor's Name (if any) _____

Your Name _____

Street _____

City _____ Zone _____ State _____

ALL UNITS FULLY GUARANTEED OR MONEY BACK WITHIN 10 DAYS

ATR PRODUCTS FOR MODERN LIVING

ATR UNIVERSAL INVERTERS

A. C. Household Electricity Anywhere . . . in your own car!

- Tape Recorders • TV Sets
- Dictating Machines • Radios
- Public Address Systems
- Electric Shavers • Record Players • Food Mixers • and Emergency Lighting.

	NET
6U-RHC (6 V.) 125 to 150 W. Shp. Wt. 27 lbs.	$66.34
12U-RHC (12 V.) 150 to 175 W. Shp. Wt. 27 lbs.	$66.34

Auto Plug-in Home-type Portable

ATR BATTERY CHARGERS

NO INSTALLATION . . . PLUG INTO CIGARETTE LIGHTER RECEPTACLE!

Keeps car battery fully charged in your own garage! Needed more now than ever before—makes motor starting easy! Operates directly from standard 110 volts A.C.current.

	NET
612CA4 (4 amp.) 6/12 V. Shp. Wt. 6 lbs.	$19.46
612CA6 (6 amp.) 6 /12 V. Shp. Wt. 8 lbs.	$22.46
612CA10 (10 amp.) 6/12 V. Shp. Wt. 10 lbs.	$27.71

ATR SHAV-PAKS

Keep Clean-Shaved! Plugs into Cigarette Lighter Receptacle. Keep in Glove Compartment. Operates Standard A.C.

- ELECTRIC SHAVERS
- Small Timing Devices . . . In CARS, Buses, Trucks, Boats, or Planes.

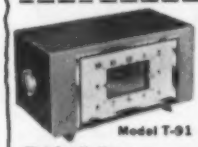
	NET
6-SPB (6 V.) 15 W. Shp. Wt. 2½ lbs.	$7.97
12-SPB (12 V.) 15 W. Shp. Wt. 2½ lbs.	$7.97

ATR ELECTRONIC TUBE PROTECTORS

Will Double or triple the life of all types of electronic tubes, including TV picture tube.

Automatic in operation, for use with any electronic equipment having input wattage of 100 to 300 watts. Fuse protected, enclosed in metal case for rugged construction and long life.

MODEL 250 (Wall Model) 115 V. A. C. Shp. Wt. 1 lb.
DEALER NET $2.63



Model T-91

MODERN TABLE ATR RADIOS

Trim, modern clock radio in ebony or ivory plastic. Powerful 5 tubes including rectifier AM radio chassis with built-in "Magna-Plate" antenna. Full-toned 4" PM speaker. Popular features include: Musical Alarm—radio turns on automatically at any pre-set time; Sleep Selector—lulls user to sleep; Automatic Appliance Timer—outlet on back of radio times any electric appliance automatically (up to 1100 watts). Cabinet 10½ in. wide, 5 in. high, 5½ in. deep. Wt. approx. 8 lbs.

Clock Specifications:

- Genuine Telechron Movement.
- Self-Starting . . . Never Needs Winding, Oiling, or Regulating.
- Simplified Clock Controls for Radio and Sleep Switch.
- 1100 Watt Controlled Outlet.
- Automatic Buzzer Alarm.
- Gold-Plated Bezel and Numerals on Large Bone-White Dial. UL Approved.

ATR HAND WIRED—NO PRINTED CIRCUITRY "TILT-A-STAND" RADIO

MOUNT ON THE WALL—UNDER A SHELF—OR SET ON A TABLE. PERFECT for every room in YOUR home.

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Letters to the EDITOR

Dear Editor:

We are real PF REPORTER fans and that's saying a lot, since my husband is the serviceman in the family, and I know nothing about electronics.

I read your magazine from cover to cover, and encircle various items of interest. The combination of PF REPORTER and my soothing telephone voice has satisfactorily handled many unhappy customers. When my husband makes the call, they tell him what a doll I am and express amazement over my technical knowledge.

Enclosed is our check for $9.00 to extend our subscription another three years. Also, please note the new mailing address. Our customers are beginning to pay us, so we can afford a better location.

HERTA GJUROVICH

Tillson TV
Tillson, N. Y.

No doubt about it, Herta, you really are a doll!—Ed.

Dear Editor:

Can you furnish me with a schematic for a Zenith TV Chassis 17T22? This is a special T chassis and I cannot find it listed in your index. I have written Zenith and contacted the local distributor; they are out of this schematic.

I am also in need of a schematic for a Model 5TB-1 transistor radio manufactured by the Victor Co. of Japan. Can you furnish the address for the importers of this radio?

I enjoy reading your magazine and think it's tops. Your service information is the most valuable tool in the department.

WM. B. WOOD

J. H. Wood Supply Co.
Hampton, S. C.

PHOTOFACT *Folder 286-13, covering Zenith Chassis 17T20, should be close enough for most purposes. Sorry, but we have no schematic for the 5TB-1; the importer is Petely Enterprises, Inc., 300 Park Ave. South, N. Y. 10, N. Y.—Ed. Thanks for the bouquets, Bill.*

Dear Editor:

I want to thank you very much for your help on a "tough dog" set. The two components you suggested checking were way off value. Replacement of these items cured the trouble.

Your magazine and your service information are worth—well, I'm stumped. How can anyone place a value on such products and information?

JOHN J. MURROW

Louisville, Ky.

Dear Editor:

Thank you for the advice on my service problem.

As I sit here with my bare face hanging out, I remember reading, in "The Troubleshooter" column, of another chap who had the same trouble with this set.

Thanks again for the helping hand.

JOE DIMOND

Casey's Appliance
Sales and Service
Port Orford, Ore.

Dear Editor:

Please send me the 1958 and 1959 Subject Reference Indexes.

I find your magazine the best in the field, and I'm happy to see you expanding your coverage to include industrial electronics.

JOHN R. MISCAVISH

J & B Electronics
St. Louis, Mo.

Dear Editor:

I am very proud of my three-year collection of PF REPORTER. It's the best in serviceman's magazines. Would you please send me reference indexes for the years '57, '58, and '59. Thanks.

WILLIS N. HOFF

Hoff TV Service
Hope, Ark.

We're kinda proud, too, fellas, of files full of similar comments. Thanks to you and all the other loyal readers who have supported us over these past 10 years.

To make your PF REPORTER *reference libraries as useful as possible, and to mark our first decade of publication, our January issue will be somewhat special. Among other things, it'll include a 16-page bonus section, indexing the entire 10-year contents of* PF REPORTER. *Don't miss it!—Ed.*

Dear Editor:

Have been buying your magazine from my distributor for the past few months, and certainly think it is one of the finest books on the market for aiding radio and TV servicemen. The articles it contains are very helpful.

G. R. BABCOCK

Janesville, Wisc.

Dear Editor:

Here is a poem which may give you a chuckle.

IMPEDANCE

Ohm's law has been accepted
And Kirchoff's has too,
But I have been rejected.
It only makes me blue.
I know the color coding
And how to align a set.
I recognize 'overloading'
But benchwork I can't get.
My technician's mind is nimble
But, for me, there is no joy.
The reason is quite simple;
I'm a girl—instead of boy!

I have been in and out of radio-TV servicing for 10 years. Reasons for being *out* are Nancy, Eleanor, Sally, and Clark, ages 3 to 13. I hope someday to write technical articles that will be acceptable in PF REPORTER.

ILAMAE V. WEBBER

San Carlos, Cal.

It's a real pleasure to hear from the top "man" in the organization.—Ed.

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13-PH2	12-H2	262 KC	Output transformer
13-PH6	12-H6	262 KC	Output transformer with diode filter
13-PC1	12-C1	455 KC	Input transformer
13-PC2	12-C2	455 KC	Output transformer
13-PC6	12-C6	455 KC	Output transformer with diode filter
13-PC7	12-C7	455 KC	Input transformer for battery radios
13-PC8	12-C8	455 KC	Output transformer for battery radios
13-PC9	12-C9	455 KC	Input transformers for AC-DC radios
13-PC10	12-C10	455 KC	Output transformer for AC-DC radios
	12-C11	455 KC	IF transformer (G.E.-RTL 143 and 163)
	12-C12	455 KC	Tapped Pri. I.F. transformer
	12-C45	455 KC	Discriminator
	13-W1	1500 KC	Input and interstage transformer
	13-W2	1500 KC	Output transformer
6203-PC	6203	4.5 MC	Input or interstage transformer
6204-PC	6204	4.5 MC	Discriminator transformer
6205-PC	6205	4.5 MC	Ratio detector transformer
6206-PC		4.5 MC	Ratio Det. (GE-RTD-026)
6207-PC		4.5 MC	Ratio Det. (GE-RTD-025)
6208-PC		4.5 MC	Ratio Det. (GE-RTD-020)
1463-PC	1463	10.7 MC	Input or interstage transformer
1464-PC	1464	10.7 MC	Discriminator transformer
	1464-WB	10.7 MC	Discriminator 900 KC Peak to Peak
1465-PC	1465	10.7 MC	Ratio detector transformer
	1465-WB	10.7 MC	Ratio detector 800 KC Peak to Peak
	6260	21.25 MC	I.F. Transformer
	6261	21.25 MC	Discriminator transformer
	6262	21.25 MC	Ratio detector transformer
6230-PC	6230	44 MC	TV Converter I.F. Transformer
6231-PC	6231	44 MC	TV First I.F. Transformer
6232-PC	6232	42.5 MC	TV second I.F. Transformer
6233-PC	6233	42.5 MC	TV third I.F. Transformer
6234-PC	6234	44 MC	TV fourth I.F. Transformer

Miniature I.F. Transformers for printed circuit transistorized applications. These miniature I.F. Transformers have tuned primary and untuned secondary windings. Proper impedance match between primary and secondary insures optimum performance.

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CAT. NO.	FREQ.	SPECIFICATIONS
2031	455 KC	10K Ohm pri. to 600 Ohm Sec., Input
2032	455 KC	10K Ohm pri. to 1000 Ohm Sec., Output
2041	455 KC	25K Ohm pri. to 600 Ohm Sec., Input
2042	455 KC	25K Ohm pri. to 1000 Ohm Sec., Output
2051	455 KC	100K Ohm pri. to 1000 Ohm Sec., Input

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Also a sub-miniature I.F. Transformer for conventional circuitry using vacuum tubes. A 455 KC intermediate frequency transformer which has all the desirable features of the standard size I.F. and is smaller than a MINIATURE tube. Through the use of a ferrite cup core these sub-miniature I.F. Transformers offer the gain and bandwidth characteristics previously obtained only in larger I.F. assemblies. For AC-DC or battery radios.

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10-C1	455 KC	Input transformer
10-C2	455 KC	Output transformer

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Miller Quality Products are recognized by the entire electronics industry as representing the finest in workmanship, performance, and dependability.

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with JFD guides, streamers, and sales helps, service-dealers get the merchandising *know-how* that nets them a bigger slice of the *3,500,000* dollar portable antenna replacement market.

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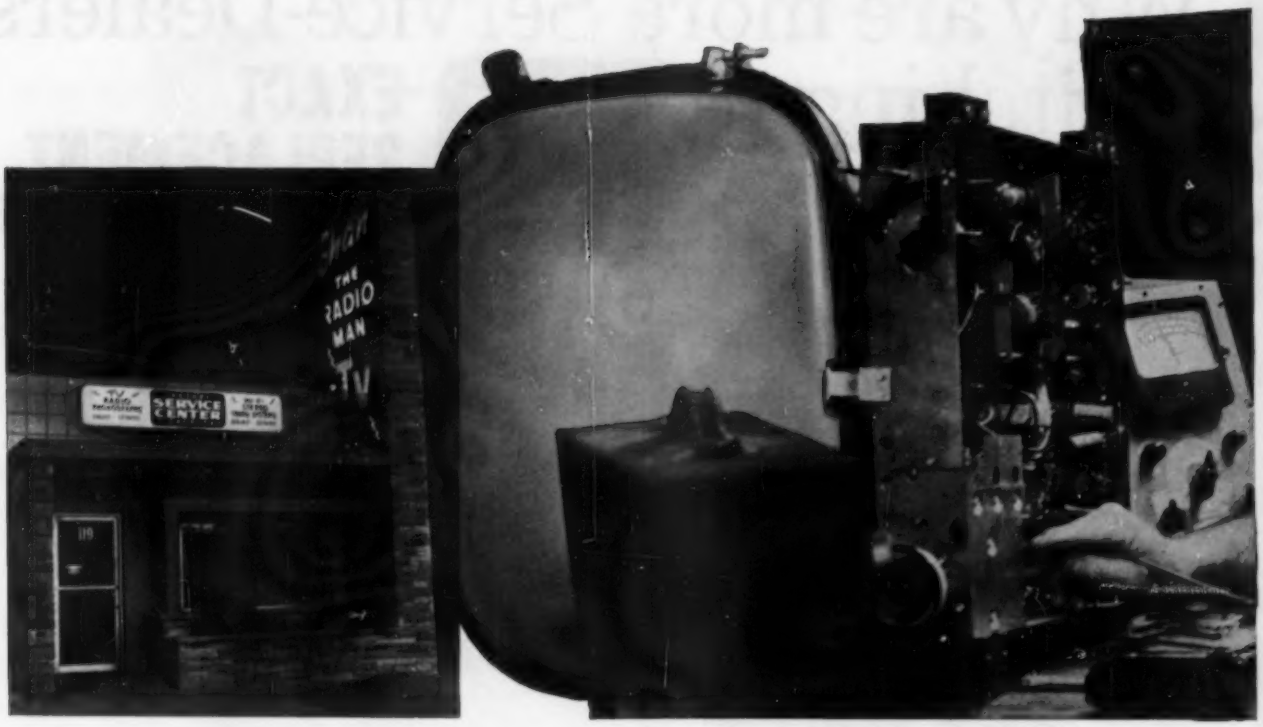

Shan the Radio Man says:

"100 years' experience

has proved we can depend on Mallory components."

"To be successful, you must make a profit, hire competent technicians, pay a fair salary, give prompt, dependable service and use the best quality components," states Shan Des Jardins, discussing the growth of his business.

"I've used Mallory components since I first started my shop. My shop people and I have a total of a century of experience and we know we can depend on Mallory for top quality components."

Shan runs an exceptional shop . . . the first in Miami to have a complete transistor radio service department, and among the first to service color TV. In all his operations, he relies on quality Mallory components. When electrolytics need replacement, for instance, he knows--as do thousands of other service technicians—that Mallory FP's give extra service in the smaller, hotter cabinets now common for TV and hi-fi . . . or when mounted next to a hot rectifier or output tube, where ordinary replacement filters wilt. They're the original 85°C capacitor. Leak-proof seal and etched cathode construction—available without premium price only in Mallory FP's—assure long life and hum-free performance.

Whatever your component needs, see your Mallory distributor. He carries the widest line of quality Mallory products . . . at sensible Mallory prices.

Shan Des Jardins is owner and manager of Shan the Radio Man Inc. in Miami. A charter member of TESA and Miami Service Association, he also is zone governor of NATESA. In 1928, Shan opened a one-man service shop for battery-powered radios. He now has five technicians and three trucks, handling 20 to 25 calls a day, servicing radio, TV, stereo and hi-fi.

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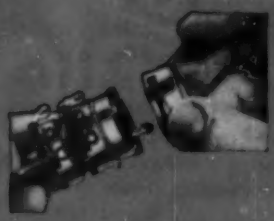

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ACROSS THE BENCH
by Stan Prentiss

"a little trouble" with an ADMIRAL 21F1

It was 10 in the morning, and the first rush of the day's service calls had tapered off to the point where I could begin to "unlax" and do some work — at least, that's what I thought. But then the phone rang, and a familiar voice piped through:

"Stan, old boy, this is Joe. I've got a little trouble with my television; if I came right over, could you throw it on the bench and fix it? I'll be glad to wait."

Intuition and experience told me, "Don't you dare!" But the hope that springs eternal in the human breast whispered that perhaps he really did have only " a little trouble." Maybe I could repair it quickly, garnering a few bucks along with some extra good will to start off a crisp winter morning. "O.K., Joe," I replied, "but which are you bringing, the Admiral or the RCA?"

"The Admiral," Joe replied. Right then and there I began to have misgivings. In the first place, I'd not seen the receiver in two years; secondly, it was a 21F1 chassis that hadn't had a capacitor changed in its nine years of existence. Mentally I saw fugitive atoms and electrons escaping everywhere. But, like all optimists who repair television sets, I still hoped for the best.

Old Buddy

Soon Joe arrived, and I put the receiver on the bench for a quick check. It had no raster, even though high voltage was present and both the B+ and boost voltages were only slightly low; furthermore, the tuner was very, very dirty. What else might be wrong I didn't know, so I asked Joe what trouble he'd been having. "Oh, some picture fading, slanting white lines across the screen . . . that's about all," he replied.

Well, now, picture fading plus retrace lines could be anything from a combination of high-voltage and picture-tube troubles to a whole string of sync, vertical, and video faults all rolled into one. These were the general possibilities — but my immediate problem was a specific point from which to start.

After a moment's consideration, I decided to measure the CRT anode potential to see if it was strong enough to produce a visible raster. The high voltage turned out to be approximately 10,000 volts—a bit short of the 12.5 kv specified by Admiral. Was it low enough to extinguish the raster? I had my doubts, and decided I'd better look for another trouble source.

I've been in this business a bit too long to panic, so I simply picked up the schematic, swung my chair away from the pesky receiver, and adjusted the fluorescent bench lamp for a bright, comfortable view. Now if a lack of high voltage wasn't killing the raster, what in the name of consternation was? Not a defective electron gun in the CRT, I hoped.

By golly, just the thought of the electron gun gave me an idea. Brightness control R2 should vary the control-grid voltage of the 17BP4 picture tube from 0 to 125 volts. I swung around in my chair, picked up the scope probe, and switched the oscilloscope's vertical attenuator so that one major division on the scale would represent 100 volts. Putting the probe on the arm of R2, I rotated the shaft of the control. Sure enough, the DC level on the scope screen dutifully rose from 0 to a little more than 125 volts. Now, I thought, how about the cathode? I touched the scope probe to the junction of R37, R38, and C26 (Fig. 1). The waveform was there, all right, but the DC voltage was far different from the 105 volts specified. Come to find out, the signal was riding at a DC level of *more than +200 volts.*

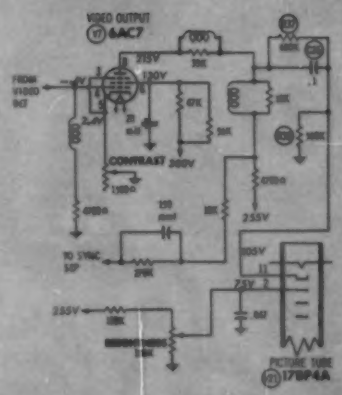
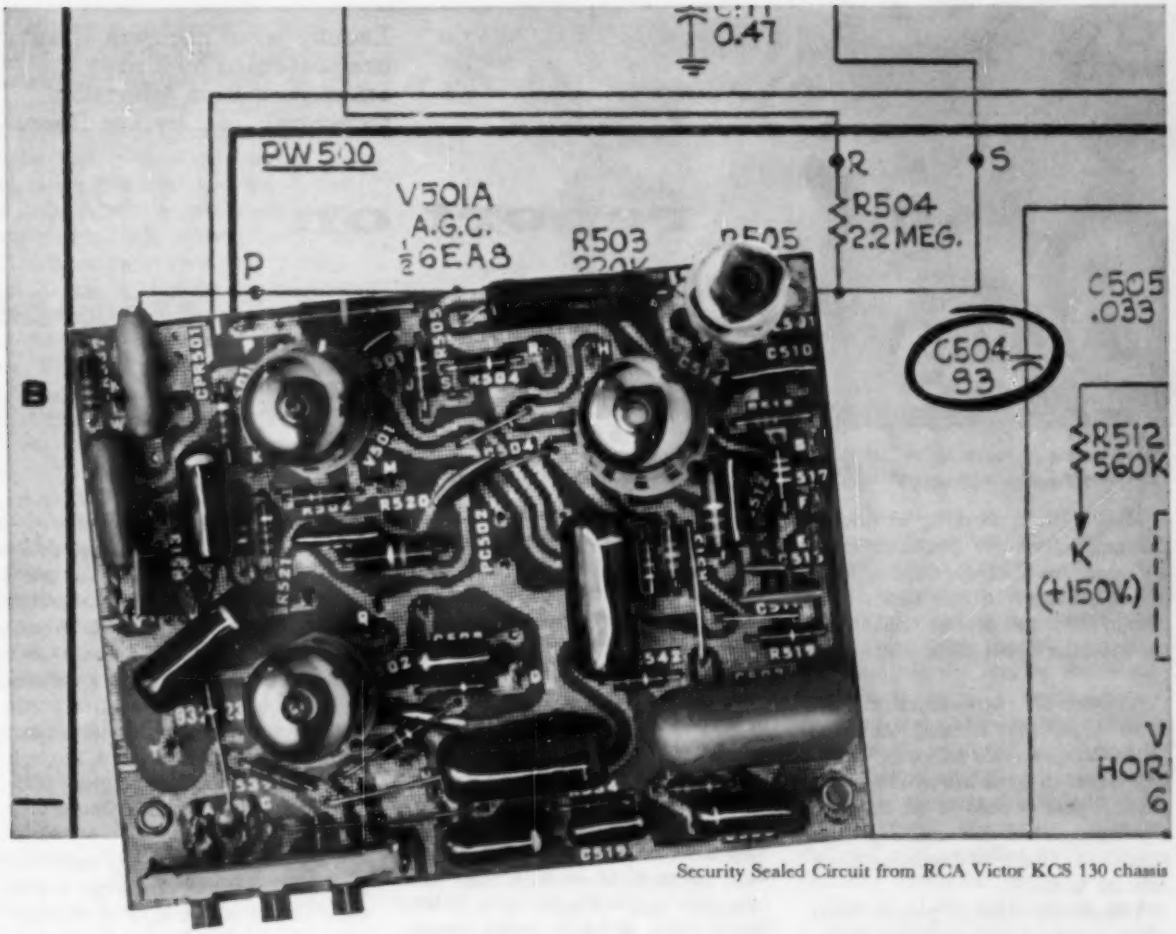


Fig. 1. Quick quiz: What faults could place 200 volts on cathode of CRT?

Hopelessly Cut Off

How could this be? Actually, there are two ways in which excessive DC voltage could reach the CRT cathode. If you follow the signal path in Fig. 1 from the plate of video amplifier V7 to the cathode of the picture tube, you'll see that R37 and R38 form a voltage divider between the plate circuit of V7 and ground, limiting the bias on the cathode of the picture tube to approximately 100 volts. The AC video signal is superimposed on this DC bias; the signal amplitude (and also, to some extent, the DC voltage) can be controlled by manual variation of the contrast control R1A in the video amplifier cathode circuit. If C26 became shorted, or R38 opened, the voltage divider would be disabled—and the full DC

• *Please turn to page 61*



Security Sealed Circuit from RCA Victor KCS 130 chassis

How fast can you find C 504?

(Average time—10 seconds)

You know how valuable minutes are in TV servicing! Every one you save means money in your pocket.

With this all-important fact in mind, take a good look at the RCA Security Sealed Circuit in the picture above. All components are plainly marked. So are meter and scope take-off points and signal injection points. RCA Security Sealed Circuits take the *guesswork* out of servicing. That's for sure!

Now compare the RCA Security Sealed Circuit with any old-fashioned point-to-point wired chassis you have on your bench. Which do you vote for as a timesaver and error eliminator? If you vote for the printed circuit, you are voting along with the nation's top missile, satellite and computer engineers! *Long ago, they chose printed circuits because printed circuits alone offer the maximum dependability.*

But, you may be thinking, how about parts replacement? Do printed circuits make this easier or tougher? The answer is—*easier!* All you need is a light, low wattage iron or gun, which is a good thing to have around the shop anyway. No special techniques are needed . . . just plain common-sense methods.

Next time a customer asks, explain that printed circuitry is the mark of modern, dependable, easy-to-service home entertainment equipment—such as RCA Victor!

TMK'59

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The Most Trusted Name in Television

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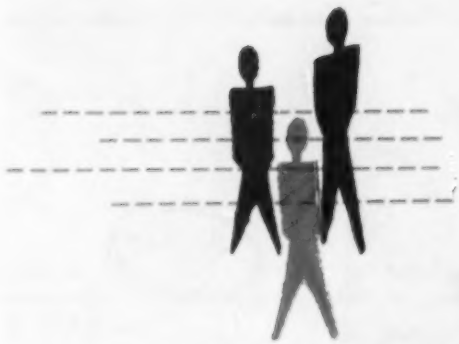
Exactly what dangers, if any, are presented by X rays emanating from television receivers? . . . by Les Deane



report on TV RADIATION HAZARDS

Fact or Fantasy?

A technician working at one of the final check-out positions on a TV assembly line develops a form of bone cancer in one hand. Is it possible that this disease could have been related to his eight-hour-a-day job?

A radio-TV serviceman experiences a periodic burning sensation about the eyes. This annoying symptom seems to grow worse with every passing year. Could it be that the big-screen TV's are emitting rays which are capable of damaging these delicate tissues?

Technically-minded people from other walks of life are often heard refusing their children front-row seats in the living-room "theater." Are they keeping their children a safe distance from the TV screen because of eyestrain alone—or are they concerned with the possibility of energy radiation from an operating cathode-ray tube?

Why should we even suspect that X rays are being emitted from a television receiver? To answer this, let's consider how X rays are produced for commercial and medical purposes.

Fig. 1. Typical radiation warning label employed on most TV picture tubes.

The X-ray tube used to generate this energy is composed essentially of a cathode and an anode in a vacuum envelope. When heated, the cathode readily emits electrons, while the anode or "target" is charged with a high positive potential — usually above 50 kv. Thus, the free electrons boiled off the cathode are traveling at an extremely high speed by the time they reach the anode. This action might be compared to what takes place in a TV picture tube, except that the electrons in the X-ray tube strike a metal target rather than a phosphor screen. The sudden stopping of electrons on the surface of the target material results in the generation of X rays. Although the accelerating potentials used in today's TV picture tubes are considerably lower than those employed in modern X-ray equipment, the voltages used in Roentgen's original discovery some 65 years ago were in the neighborhood of only 20 kv. From this we can see why many people acquainted with X-ray phenomena support the belief that there *could be* radiation from the cathode-ray tubes used in television receivers.

The TV serviceman is made aware of possible radiation through statements appearing in tube manuals and even by warnings on the CRT's themselves. (See Fig. 1.) It's quite natural for some of us to become a little alarmed upon reading these notices when we realize that many TV picture tubes are now operated at anode voltages above 16 kv.

What are X rays?

Before going too far with our discussion, the term "X ray" should be properly defined. X rays are nonluminous electromagnetic radiations of extremely short wavelengths, produced by bombarding a substance with electrons moving at great velocity. X rays are capable of penetrating opaque or solid substances, ionizing gases and tissues through which they pass, and affecting photographic plates and fluorescent screens.

This invisible, wave-like radiation represents a form of energy somewhat similar to the rays of ordinary light. Comparing X rays to RF frequencies, we might say that their spectrum extends from about 3 x 10^{10} mc to 3 x 10^{16} mc. Naturally, at these extremely high frequencies, their wavelengths are microscopic. The penetrating power of an X ray depends largely on its wavelength; the shorter it is, the more effective it becomes. X rays are often classified as either "hard" or "soft"—those with more intense energy or

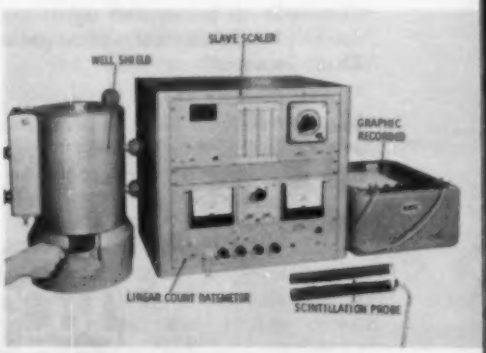


Fig. 2. Type of test equipment used for our TV radiation measurements.

penetrating power being the harder.

The density of X-ray radiation is proportional to the density of the material which emits it; therefore, if X rays are to be generated, the two major factors involved are the accelerating potential and the nature of the substance or substances under bombardment. It is the property of all such substances not only to transmit X rays in varying degrees, but also to absorb and scatter them in all directions. In the case of a CRT, we are concerned with materials such as specific types of glass, phosphor, and aluminum—of which little is actually known with respect to X-ray behavior.

A common unit of measure for X-ray radiation is the *roentgen* (r), which expresses radiation in terms of the amount of ionization produced in air by the X rays. The *milliroentgen* (mr) is one thousandth of a roentgen. Energy levels of such radiation are expressed in electron-volts, or more often in thousands of electron-volts (kev).

Lab Test Procedure

When I began research on this subject, I was forced to swallow a pinch of salt with every opinion I heard, because no one was able to conclusively substantiate his theories with factual findings. Many said that, if X rays are generated within a CRT, they would never be capable of penetrating the relatively thick glass. Some were firm believers that, since electrons strike the front screen with such great force, some are bound to pass right on through. Others contended that there would probably be more X-ray radiation at the neck of the tube, where some electrons pound against metal parts of the gun assembly. Still others had the idea that X rays are more likely to be given off at the high-voltage rectifier tube.

After making a fruitless effort to obtain some authoritative data on this controversial subject, we decided that the only way to prove or disprove the theory of harmful radiation from TV receivers was to perform a series of practical tests. By combining the technical know-how of both TV technicians and radiation specialists, we hoped to come up with the answers.

Our initial problem was to contact qualified personnel and to arrange for the use of the most suitable equipment for our highly specialized tests. Fortunately, Nuclear Measurements Corp. here in Indianapolis, who manufactures precision radiation-measuring and detecting equipment, was kind enough to give us full cooperation with this research program.

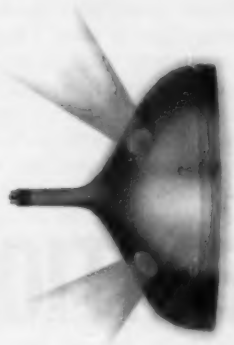


Fig. 4. Two radiation "hot spots" found on each side of the CRT bulb.

Fig. 5. Mr. W. H. Bradley, president of NMC, probes a tube for X radiation.

A Geiger counter was neither sensitive nor accurate enough for our particular radiation measurements. The type of measuring equipment employed for this project is shown in Fig. 2. This *gamma spectrometer* system is capable of detecting, tracing, and identifying radiation down to very low energy levels. The system offers three different forms of monitoring or readout: Counts per given time cycle, continuous counting rate, and permanent graphic recordings.

The *scintillation probe* in Fig. 2 is a portable radiation detector. Basically, radiation enters through a "window" at the end of the probe and reacts upon a spectrometer-grade crystal. The crystal gives off light energy in direct proportion to the radiation energy. A photomultiplier tube converts this light to electrical pulses, which are in turn detected and amplified by transistor circuitry within the probe.

Output of the scintillation probe is coupled to a *linear count rate-meter*, which detects the radiation and provides a continuous meter reading of relative energy. In addi-

• *Please turn to page 56*

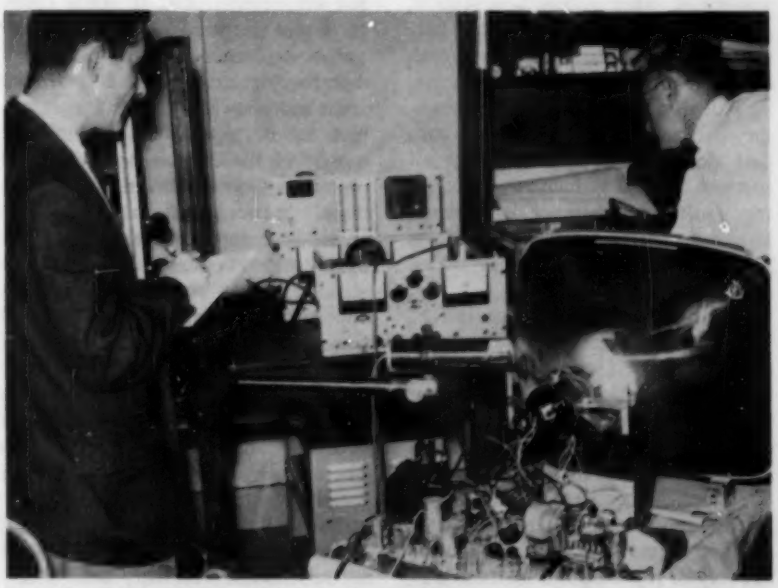


Fig. 3. A test setup which helped us find answers to the X-ray question.

REGENERATION IN PICTURE-SIGNAL CIRCUITS

by Allan F. Kinckiner

How to diagnose, localize, and cure spurious oscillations in video IF and related stages.

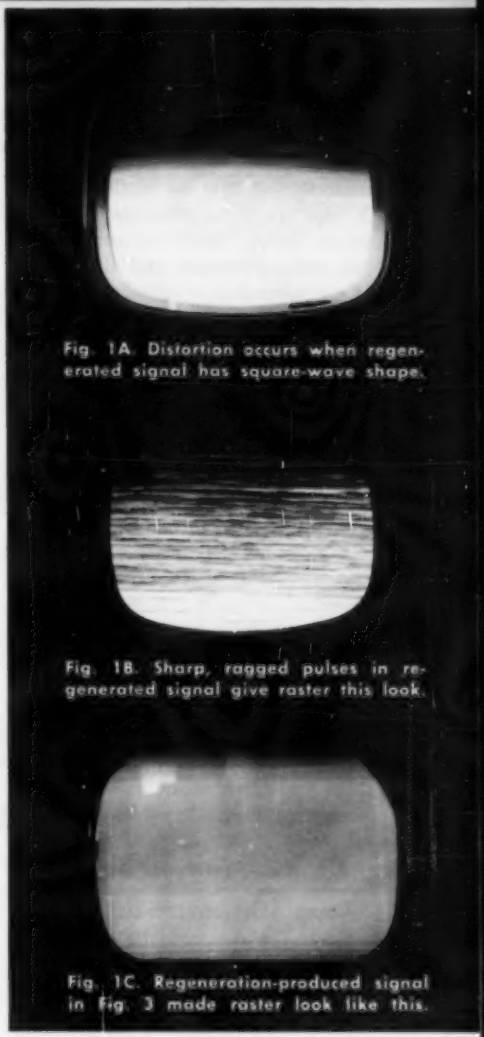


Fig. 1A. Distortion occurs when regenerated signal has square-wave shape.

Fig. 1B. Sharp, ragged pulses in regenerated signal give raster this look.

Fig. 1C. Regeneration-produced signal in Fig. 3 made raster look like this.

The trouble commonly called "regeneration" is also known by a variety of other names (oscillation, feedback, looping, etc.), but whatever term a serviceman may use to describe this unwelcome condition, he is likely to add an uncomplimentary adjective. Regeneration can, and does, occur in practically all sections of a TV receiver, producing confusion wherever it appears. However, its most baffling effects are observed in those stages whic' handle the picture signal.

The results of regeneration in RF, IF, or video circuits can show up in the picture itself, the most common symptoms being poor definition and ghosts. The same basic trouble can also lead to erratic horizontal and vertical sync, or to supercritical fine tuning. Furthermore, since the picture and sound signals are jointly handled by many of the same amplifier stages, regeneration in these circuits also affects the sound. The audible symptoms vary considerably; rushing or panting noises are not uncommon, and in some cases the effect is almost identical to ignition noise in an auto radio. Since the disturbances in the sound generally seem more severe than those in the picture, customers may complain mostly of the excessive noise being created—even if this noise occurs mainly between stations.

Because regeneration is masked or swamped out by strong input signals, it often assumes the appearance of intermittent trouble. Operation may be normal except when a change in atmospheric conditions or antenna orientation produces a drop in RF signal level; then the raster becomes broken up or distorted. The appearance of the screen varies greatly from case to case, as illustrated by the three examples in Fig. 1 (all taken with antenna disconnected). Some receivers that operate normally with rooftop antennas will suffer from raster breakup if operated with rabbit ears; on the other hand, some portables will not function correctly with their own antennas, but will present a faultless picture if an outdoor antenna is attached.

From this behavior, we can conclude that the presence of regeneration can be verified by merely disconnecting the antenna. A "breakup" symptom in place of a clean, slightly snowy raster (Fig. 2) not only proves regeneration is taking place, but also represents a steady-state trouble condition which can be isolated and corrected. (In some high-noise areas, it might be necessary to short across the receiver's antenna terminals to prevent variations in random noise from affecting the regenerative condition.)

Another method of determining the presence of regeneration and localizing its cause is to measure the voltage across the load resistor of

Fig. 2. Normal raster with antenna disconnected means "no regeneration."

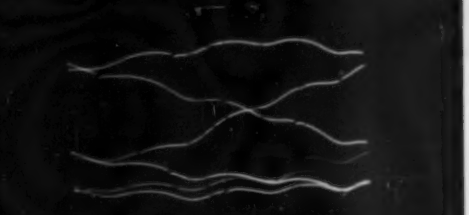


Fig. 3. Wildly distorted video input to the CRT in the case of Fig. 1C.

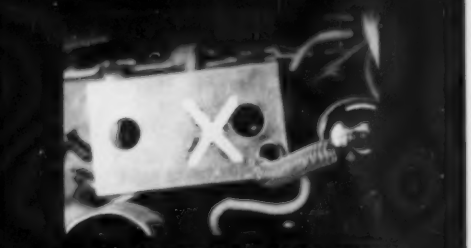


Fig. 4. "X" marks the shield responsible for regeneration in RCA KCS109.

the video detector. This test, made with no antenna connected to the set, should normally result in a maximum reading of minus 1 volt DC. An output of several volts not only proves that regeneration is taking place, but also shows it is being developed somewhere between the RF input and video detector. Regeneration in the video amplifier can be localized by disabling the last IF stage. If regeneration is occurring in or after the video detector, it will show up as distortion somewhat like that in Fig. 1.

To localize the trouble still further, we can check the video IF stages with a typical alignment setup using a sweep generator and scope. If the IF bandpass curve looks normal when the generator output is strong, but breaks up into jagged peaks and valleys when the sweep-signal amplitude is decreased, regeneration in the IF section should be suspected.

Looking at the input waveform to the picture tube when regeneration is present explains why the raster or sound distortion can take so many different forms. The scope trace shows that regeneration - produced signals can have any number of different shapes——an almost square-wave pulse in the case of Fig. 1A, a sharp pulse for Fig. 1B, and the "you-name-it" pulse in Fig. 3, corresponding to Fig. 1C. From this, you might conclude that scope troubleshooting is not much help in these sets; but it can sometimes be of real value, as the following example will prove.

At first the raster shown in Fig. 1C was believed to be the result of vertical trouble, or a feedback loop between the vertical and video-signal sections, but the scope quickly indicated that such was not the case. The distortion evident in Fig. 3 was still present even when the vertical sweep tubes were removed. Further troubleshooting proved that the regeneration was caused by a positive-feedback loop from the sync and keyed AGC stages back to the video amplifier. The condition was cured by adding a decoupling network at the screen grid of the video amplifier. Voltage had previously been fed to this element from a source common to the screen grid of the keyed AGC tube.

Cases, Causes, and Cures

The simplest regeneration-creating condition is brought on by a tube which provides too much gain —one with an "overactive thyroid," as one serviceman described it. At the other end of the scale are the complex, hard-to-find problems involving positive feedback loops due to faulty lead dress. Between these extremes is an assortment of other causes—some easy to correct once they are located, others not so easy.

Surely everyone who has been in the service business for very long has experienced a case of regeneration due to extra-high transconductance in a tube. Most such occasions are well remembered. In my own experience, this fault has occurred most frequently in Admirals of the 1950-52 period.

One of my earliest and most memorable bouts with regeneration was experienced with a 7" Philco. The chassis had never been out of its case, and the customer claimed he had not so much as removed the back. Yet, here it was on the bench with a classic case of raster break-up due to regeneration. This, in turn, was due to a shield missing from a 6AU6 sound IF tube — which was in a virtually inaccessible location even with the chassis pulled out for inspection!

Resistor Changed in Value

A more recent case involved an RCA portable using Chassis KCS109C—a late-production version of this chassis with three IF's. The customer had had his set serviced by another technician who had replaced the 6CU8 third IF tube. The set worked well with an outside antenna, but when the built-in antenna was employed, the picture sporadically broke up as in Fig. 1A. Completely removing the antenna caused the condition to be displayed continuously. A diagnosis of IF regeneration was verified by hooking a sweep generator and scope to the set.

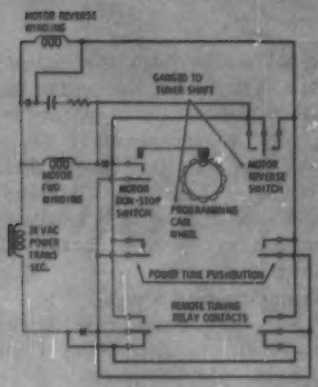
To my relief, I had good luck on this set. Here's how I went about finding the trouble: With the sweep-generator output decreased to the point of waveform breakup, I started changing tubes, eyeing the waveform all the while. In doing so, my attention was focused on two well-browned resistors. Going to work on these, I found they were cathode-bias resistors in the first and third IF stages, respectively. The former (a 47-ohm unit) had increased to 150 ohms, while the other had risen from 180 to 500 ohms. After replacing both resistors, I repeated the sweep-generator test and found that the regeneration had been corrected.

My guess was that the cathode resistors had been damaged by a shorted tube or tubes; this explained why the third IF had recently been replaced. The reason why this trouble produced such odd behavior is just a calculated guess. I have an idea that the entire video IF strip may have acted somewhat like a multivibrator under weak - signal conditions, with the necessary regenerative signal being fed back from the video detector by way of the AGC filter and bias network.

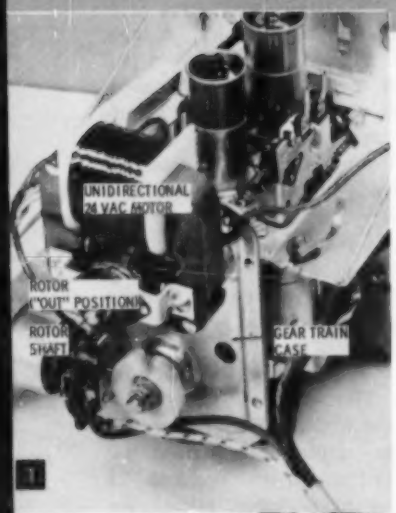
Poorly-Grounded Shield

Another RCA portable, by coincidence also a KCS109, was re-

• *Please turn to page 65*



EXAMINING MOTORIZED TUNING MECHANISMS



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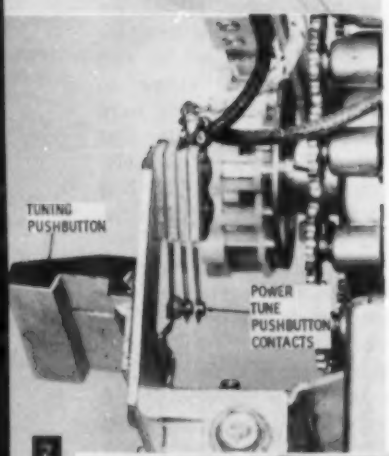


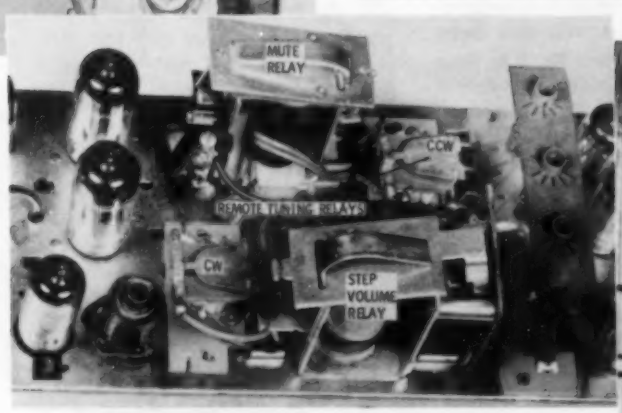
2

Channel selection may be either bidirectional or unidirectional; that is, the tuner may rotate in either direction, or in just one—from low to high. The heavy lines in the circuit diagram indicate the additional circuitry required for bidirectional operation. While many different switching systems are used, all are similar to the one shown here, and follow the same general principles of operation. Depressing a push button supplies power to the motor from a secondary winding on the power transformer. As soon as the motor is energized, a run-stop switch automatically closes, keeping the circuit closed until the next "on-channel" position is reached.

The 24-volt split-phase motor requires a starting capacitor, in series with a resistor across the winding, in order to develop the required torque. If control is bidirectional, a second motor winding is used for reverse drive. When the motor is energized, the rotor engages a gear train that drives the tuner shaft. When the motor stops, the rotor returns to an "out" position (photo 1), disengaging the gear train.

The tuning cycle begins when either the power tuning push-button contacts (photo 2) or one of the remote tuning relays (photo 3) are closed. Although these switch devices are often located at some distance from the motor assembly, they can be easily identified by their basic physical characteristics.

Some manufacturers use the rotor end-play action to also perform one or more of the switching functions. In photo 4, end-play action closes the motor run-stop contacts and opens a pair of muting contacts when the motor starts. When the motor stops, the spring-loaded rotor returns to the "out" position, opening the run contacts and closing the audio contacts.



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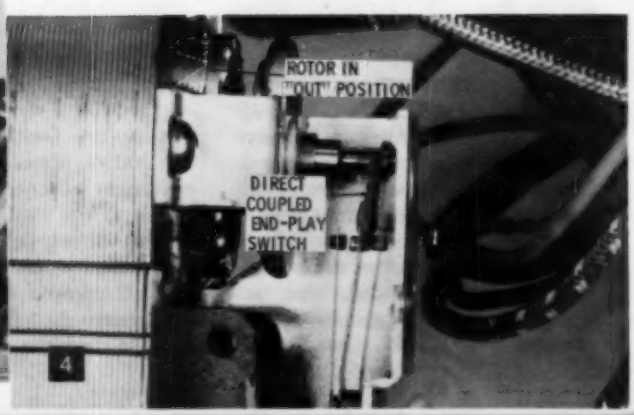
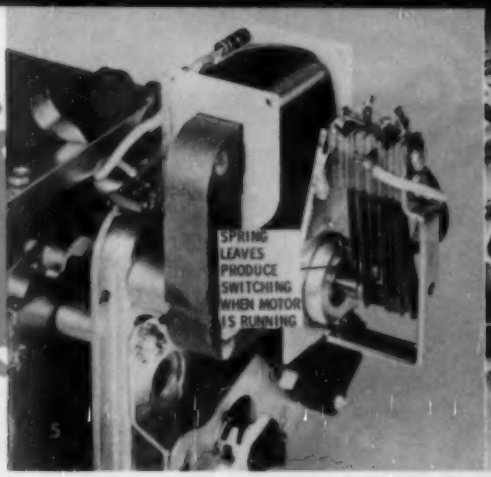
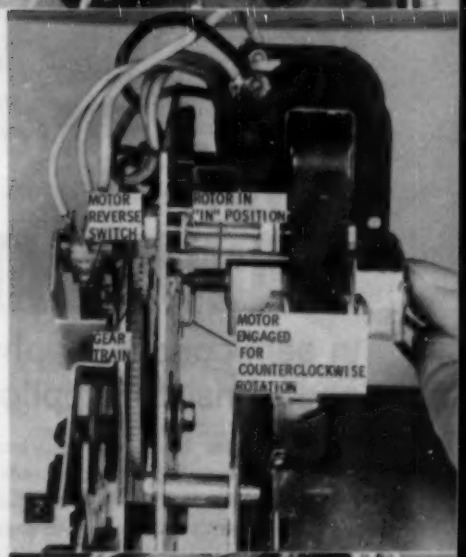


4

Power TV tuning units have grown in popularity until, today, every major manufacturer has at least one remote-control or power-tuned receiver. The accompanying photos will give you a close-up view of the "muscles" in modern motorized tuning mechanisms.



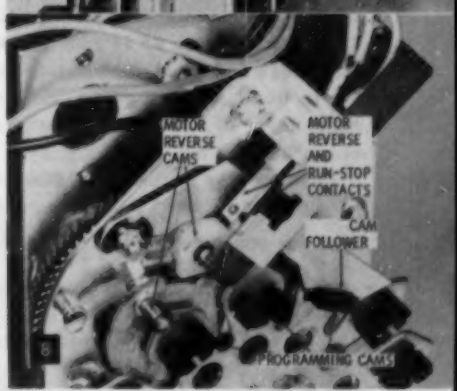


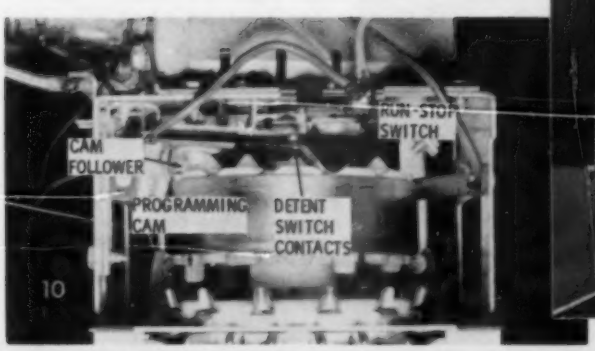
The three-gang end-play switch in photo 5 depends only on the spring action of the leaf switch to close the contacts when the motor runs, and closes an additional set of contacts to bypass the circuit-activating switches.

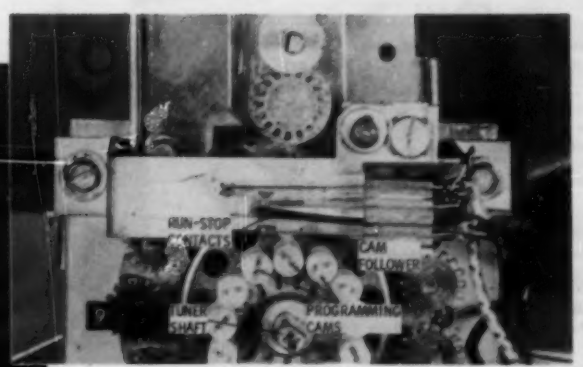
In bidirectional systems, after the initial starting action, some form of motor-reverse switch is employed to keep the proper motor winding connected into the circuit. Photos 6 and 7 show the methods used to properly position the switch contacts. While there are minor variations from these designs, all use rotor torque to drive a mechanical linkage which closes the correct contacts before the initial contact is broken.

One of the major differences between units is in the programming system. In the mechanism of photo 8, the motor-reverse contacts double as motor run-stop contacts. They are opened by the cam-follower arm when the cam is in the flat position, thus breaking the circuit and stopping the tuning cycle. The cam system in photo 9 operates just the opposite of the one shown in the schematic. With the flat part of the cam toward the switch contacts, the motor continues to run; when the rounded part is toward the contacts, they open the motor-run circuit. The other two sections of the leaf switch disconnect the audio and darken the picture tube while channels are being changed.

Two separate sets of switch contacts are used with the programming wheel in photo 10. The contacts of the conventional run-stop switch are hidden by the cam that actuates them; however, the special detent-switch contacts are clearly visible. This unit is used with tuners which do not have a stiff detent spring; the detent switch is wired in parallel with the run-stop switch to provide precision stopping.







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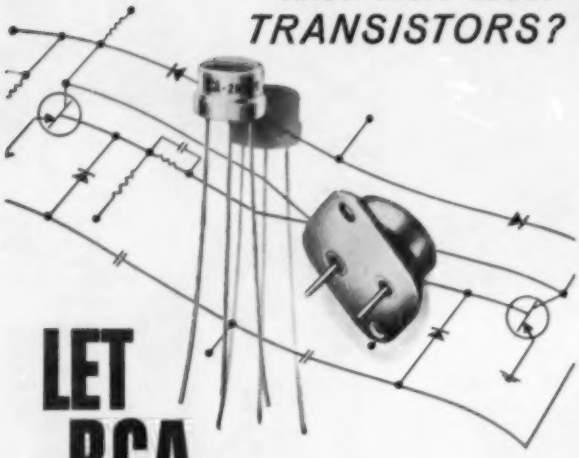

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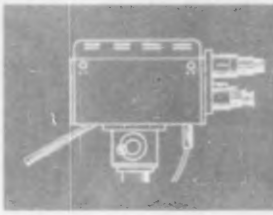

The Electronic Scanner

Premiums Galore

Service aids, toys, cameras, watches, and other useful items for home and shop are among the 17 valuable premiums available with the purchase of **RCA** receiving tubes. Heading the premium list in this "Front Page Program" is the Meter Chest, a 200-tube caddy equipped with **RCA's** WV-38A VOM.

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Owners of **B & K** tube testers may obtain setup data on new tube types from **B & K Mfg. Co.** The "New Tube Information Service" is issued by the manufacturer every 3 months. An annual subscription includes all 4 issues for $2.50. Single copy price is $1.50.

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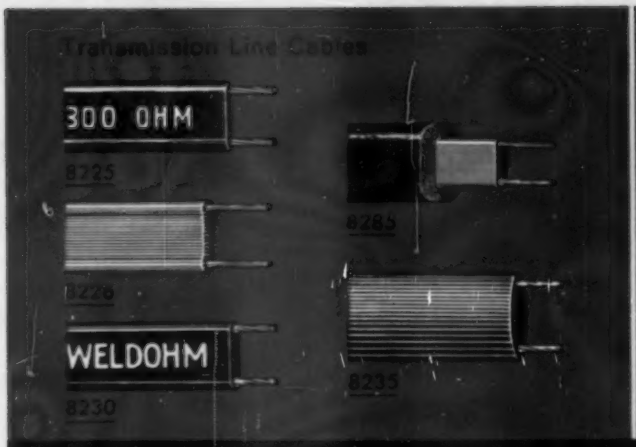

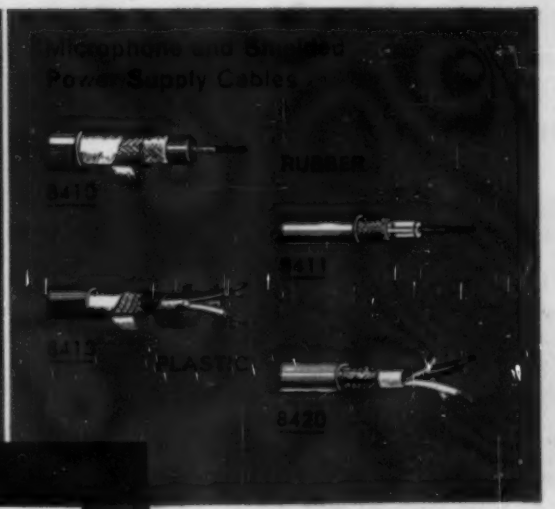

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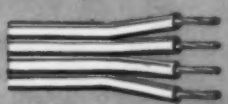
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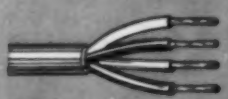
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How do you rate? Not long ago an appliance service survey was conducted in a leading metropolitan area to determine customer reaction to the cost, quality, and speed of service received. While radio and television service differs in many respects from appliance service, customer reactions are prone to follow the same patterns in both cases. Some very interesting facts came to light. For one thing, the survey showed that a healthy percentage of newly-purchased items required service during the first year, which indicates the necessity for keeping abreast with new designs.

Questioned about the promptness of service, nearly one out of four people felt they received slow service. Of these, almost half thought this was because the service organization didn't have the required parts in stock, while over a third felt the call just wasn't handled as promptly as it should have been. These are the dissatisfied customers whose business is ready for "wooing." That one-fourth of the country's consumers feel this way is appalling.

The feelings regarding quality and promptness dovetailed when cost was brought into the picture. Two-thirds of the group polled felt the service they received was both prompt and satisfactory; only 7% of these folks thought the charges were high. On the other hand, among the third who felt service was generally poor or slow, 24% were of the opinion that the cost was too high. It's the same old story: When people receive *good* service, they rarely complain about price. How do *you* rate?

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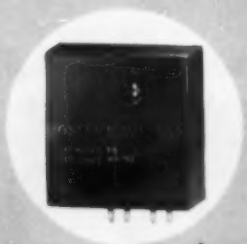

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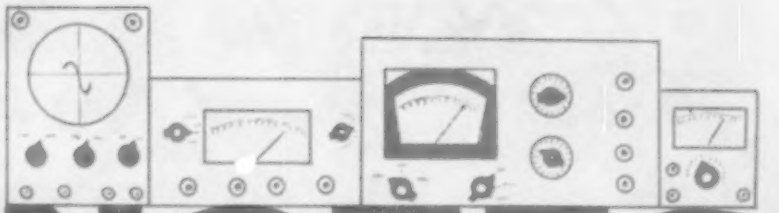
WT-14	13.8-16
WT-21	16-28
WT-41	27-55
WT-78	47-110
WT-165	100-230

Mosley Electronics, Inc.
St. Louis, Missouri



NOTES ON TEST EQUIPMENT

by Les Deane

Farad Finder

The instrument pictured in Fig. 1 is designed expressly for measuring capacitor values. Manufactured by Arkay International, of Richmond Hill, New York, the Model CA-40 Capacity Meter is a direct-reading instrument well suited for radio and TV service work as well as laboratory and industrial applications. The unit comes complete in either kit or factory-wired form.

Specifications are:

1. *Power Requirements — 105/125 volts, 50/60 cps; power consumption approx. 25 watts; transformer provides line isolation.*
2. *Capacitance Range — five switch positions provide full-scale ranges of 50, 100, and 1000 mmf, .01 and 0.1 mfd; special test jack provides additional range of 0.1 to 1.0 mfd.*
3. *Calibration — five individual calibrating controls provided; precision calibrating capacitors available.*
4. *Other Features — 6" 50-ua panel meter with two scale arcs for all six ranges; two 30" test leads supplied.*
5. *Size and Weight — case 6½" x 7¾" x 4¼", 4½ lbs.*

At first glance, this unit looks somewhat like a VTVM. It is housed in a black *bakelite* case and has an all-metal front panel. The wide-angle meter occupies the top half of the panel, the lower half serving as a mounting plate for an off-on switch, capacitance range selector, and three test terminals. Each terminal on the panel is a combination banana-plug jack and universal binding post. The test leads are equipped with banana plugs on one end for connection to the meter, and alligator clips on the other end for connection to capacitors under evaluation.

To measure capacitance, you merely select the proper range and connect the questionable capacitor across the test leads. A value between 1 mmf and 1 mfd is then indicated directly on the appropriate meter scale (MMF or MFD). The instrument is not designed for in-circuit testing, nor is it intended to measure electrolytics, since they have very high leakage characteristics. Accuracy of its readings depends largely on how precisely the meter is initially calibrated. After calibrating the Model CA-40 with capacitors of ±.5% tolerance, I found it to be as accurate as some of the more expensive bridge-type instruments.

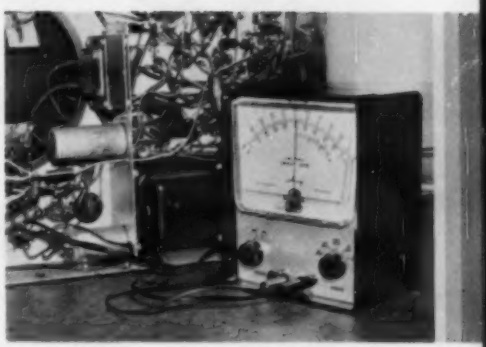


Fig. 1. Arkay's new meter measures capacitor values from 1 mmf to .1 mfd.

A complete circuit of the CA-40 is shown in the schematic of Fig. 2. Dual triode V1 functions as a cathode-coupled multivibrator which supplies a pulsating output across cathode resistor R7. Capacitors C1 through C5 provide a means

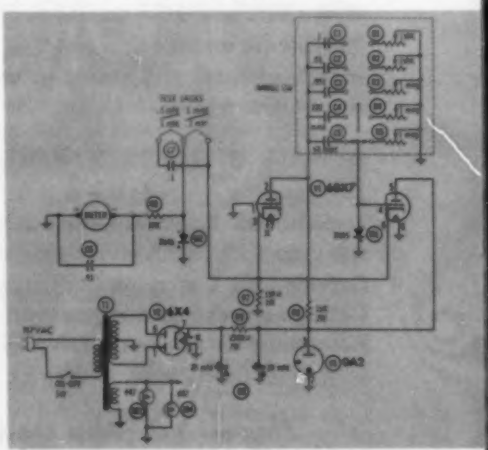


Fig. 2. The CA-40 consists of an oscillator, meter circuit, and power supply.

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for altering oscillator frequency, and potentiometers R1 through R5 are used for the calibration of each range. Diode M1 provides a low resistance charging path for the oscillator coupling capacitor, thus eliminating R7 from the charge path. Consistent pulse amplitude and stable operation of the oscillator are assured by the use of a regulated plate supply voltage.

As illustrated in Fig. 3, output of the multivibrator is developed across cathode resistor R7 and applied to the unknown capacitor. The positive-going pulse of the applied signal (W1) causes the meter rectifier M2 to conduct and charge the unknown capacitor. Between pulse intervals, M2 ceases to conduct, and the capacitor discharges through the meter circuit. The meter reading thus provides a direct indication of the charge stored by the unknown capacitor. With a damped meter movement and components R8 and C6 acting as filters, the reading obtained represents the average value of the pulse signal (W2).

Since the amplitude of the multivibrator signal and the impedance of the metering circuit are relatively constant, frequency of the test signal is made variable to compensate for the different capacitance ranges. For example, the multivibrator frequency is increased by 10 times when changing the range setting from full-scale indications of .1 to .01 mfd. Hence, repetition rate of the charging pulses increases as capacitance of the measured component decreases, and the meter is calibrated accordingly.

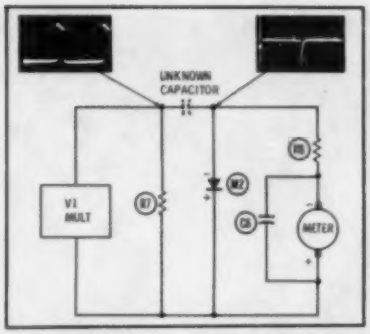

Fig. 3. Diagram showing operation and test signal of the Capacity Meter.

Since the Model CA-40 is a direct-reading instrument and its operation is so simple, I found it ideal for quick measurements of stock parts. It would also be useful in production line work. I've found such an instrument very helpful when trying to pinpoint the cause of frequency drift or phase shift in an oscillator circuit. For instance, if a capacitor is changing value in a horizontal or vertical oscillator stage, about the only way to find it is by direct substitution or through an accurate measurement of its value. The precise value of a capacitor is not always of concern in ordinary coupling or bypass applications, but when it comes to tuned stages or wave-shaping networks, this factor is extremely important.

Portable Service Shop

Mercury Electronics Corp., Mineola, New York, has recently introduced a new instrument that accomplishes the work of several. The Model 300 Combination Tester shown in Fig. 4 incorporates a multiple-socket tube tester, picture tube tester-reactivator, and a VOM section that measures voltage, current, resistance, and capacity.

Specifications are:

1. *Power Requirements — 105/125 volts, 60 cps; AC power consumption less than 5 watts standby; power indicator on front panel; transformer provides line isolation; self-contained 1.5- and 6-volt batteries supplied.*
2. *Tube Tester — checks over 700 different tube types for shorts, leakage, gas, and emission; 17 prewired test sockets provided on panel; shorts and leakage indicated by neon lamps; built-in 7- and 9-pin straighteners; tube chart supplied and new listings furnished to registered owners.*
3. *CRT Tester — tests both monochrome and color picture tubes for leakage, shorts, and emission; provides tests for types with 2.35-,*

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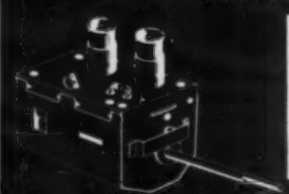

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7. *DC Ammeter — five full-scale ranges of 75 ua, 7.5 ma, 75 ma, 750 ma, and 15 amps; leads and terminals color-coded for polarity.*
8. *Capacity Meter — capacitor values including electrolytics indicated on two ranges of from .001 to .5 mfd and 1 to 80 mfd; calibration adjustment and* HI-LO *range selector provided on panel.*
9. *Size and Weight — case 17½" x 13⅛" x 4½", 12½ lbs.*

From the long list of specifications, you can easily see where the *Combination Tester* gets its name. The instrument is mounted in an attractive hand-rubbed oak case with detachable lid. A metal spring clip is attached inside the lid for securing the tube-data binder and instruction manual supplied with the unit. The instrument's case also includes a storage compartment for tools, test leads, and cables.

Although the panel meter is loaded with scales for the various functions and ranges, its wide-angle D'Arsonval movement makes it easy to read. The meter measures 6" across and is heavily damped.

After making use of the Model 300 in the lab the past few weeks, I found it to be a very versatile instrument — yet one that presents no problem at all when switching from one application to another. I'm often skeptical of instruments which claim to do a number of different jobs, because in many cases it may require too much time and effort to convert the unit from one mode of operation to another.

Fig. 4. A tube and capacitor checker, VOM, and CRT restorer all in one unit.

This is not the case with the Model 300; in the center of its panel, directly below the meter, is a 4-position master switch which enables you to select the proper function with a twist of the wrist. There is also no interaction between test sections, and therefore less danger of in-

Fig. 5. Portion of the Model 300 panel devoted exclusively to CRT testing.

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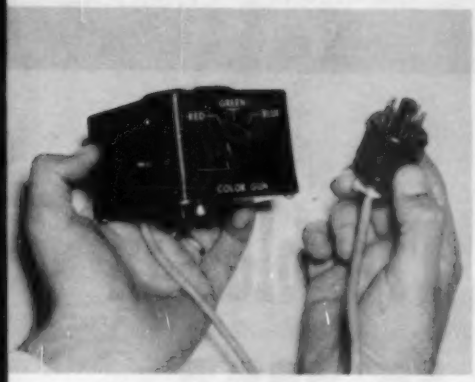

Fig. 6. The CRT test cable supplies 4 individual sockets for all tube types.

strument damage.

Not having space to give you a report on all my experiences in the various applications of the Combination Tester, I've singled out the picture tube tester-reactivator for your particular attention. The instrument panel is divided into three major sections — tube testing, VOM functions, and CRT testing. The entire CRT section is shown in the close-up photo of Fig. 5.

To test a picture tube, the master switch is placed in the CRT position and AC power is applied. The selector switch in the center of the CRT section is then turned to the position labeled FIL CONT. The LEAKAGE-QUALITY slide switch (lower-right of Fig. 5) is positioned on LEAKAGE; and the FILAMENT VOLTAGE switch (lower left) placed in either the 8-, 6-, or 2-volt position, depending on the filament rating of the tube being tested.

The octal plug of the *Multi-Head* socket adapter (Fig. 6) is connected to the socket at the bottom of the CRT panel. The picture tube is then connected to the proper base socket at the other end of the adapter cable. Note that on one end of the *Multi-Head* unit there is a color gun selector. This switch permits you to test or reactivate each gun of a color tube separately.

With the instrument set up in this manner, the yellow-jeweled lamp labeled LEAKAGE will glow immediately if the tube's filament is intact. To check for shorts, the selector switch is advanced to the remaing four positions — G-1, G-2, G-4, and CATHODE. If the leakage lamp glows steadily, either a short or leakage of less than one megohm is indicated.

For an emission check, which can also help to detect an open element, the selector switch is placed in the G-1 position, and the LEAKAGE-QUALITY switch in the QUALITY position. Relative emission will then register on the BAD-REACTIVATE-GOOD scale of the panel meter.

Two modes of CRT reactivation are offered by the Model 300: One is a "boost method," which increases heater voltage by 30%; and the other is a "shot method," which employs approximately 1000 volts DC to clean the cathode coating or to weld a shorted or open element. The reactivation circuits are energized by the small red button in the upper-left corner of the CRT test panel. ▲

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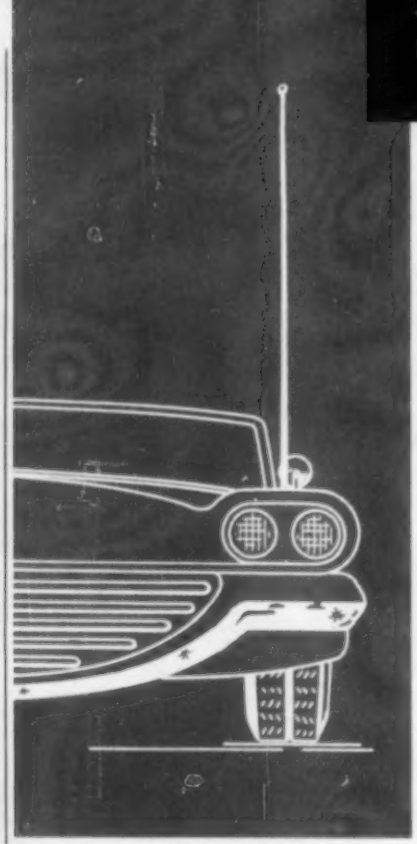

Troubles in 57 FORD Radios

We're not deliberately picking on a certain model — but we have noticed an unusually large number of troubles in the 74BF and 75BF auto radios used in 1957 Fords. There are several reasons for this. One is the popularity of the car itself, leading to a large quantity of these radios in the field; the other is that 1957 was the first full year of hybrid-radio use. Some of the following troubles occur in enough different radios to be of special interest; in other cases, the trouble is more unusual, but still interesting.

Open Emitter Resistor

As you may have already recognized, these are the models that use a piece of special wire several inches long to produce exactly 1 ohm of resistance in the emitter circuit of the output transistor. As Fig. 1 shows, the emitter returns to the 12-volt battery supply, so the 1-ohm resistance is in series with the output transistor and collector-circuit transformer across the source. Besides serving as a check point for proper emitter current, the 1-ohm resistor—although not specifically designed to act as a fuse—also helps protect the transistor in case of heavy current overload.

We have taken in several of these radios with the 1-ohm wire burned open; as fast as we put in replacements, they also burn open. In a surprisingly large number of radios, we have found the cause of this trouble to be a shorted spark plate at the center tap of the output transformer (Fig. 1). The resulting current increase is not great enough to ruin the transistor, since the output (collector) circuit is not completely shorted; however, enough extra current does flow to take the resistive wire out.

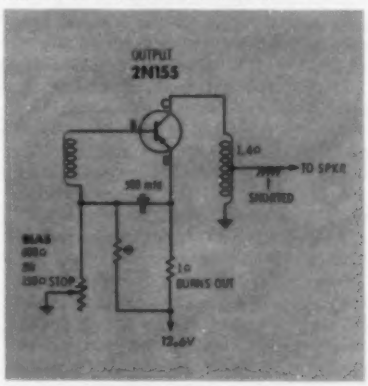

Fig. 1. Emitter return of output stage in Model 74BF is through 1-ohm wire.

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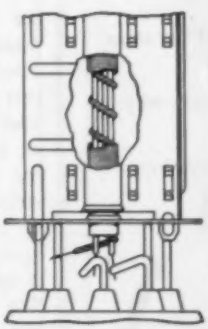
I won't bore you with all the details. But typical of my many new design features is my anchored heater-cathode insulator. Actually a tungsten coil coated with insulating material, it is mechanically anchored to prevent any movement that might cause me heater-cathode shorts. This coil also has fewer turns to minimize cathode-to-insulator contact . . . yet keep my heater-cathode spacing perfect.



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The "Big Picture"

... informative shop talks

by AL MERRIAM

Sylvania National Service Manager

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SERVICE TIP OF THE MONTH

Symptom (Effect)—Squegging (horizontal oscillator "takes off" at some odd frequency) accompanied by a squealing sound.

Cause—Antenna picks up radiated pulses from scanning system which disrupts AFC network.

Cure—Increase the value of the cathode resistor of the horizontal oscillator from 1000 ohms to 1200 ohms or slightly higher.

Sylvania Home Electronics Corp., Batavia, N. Y.

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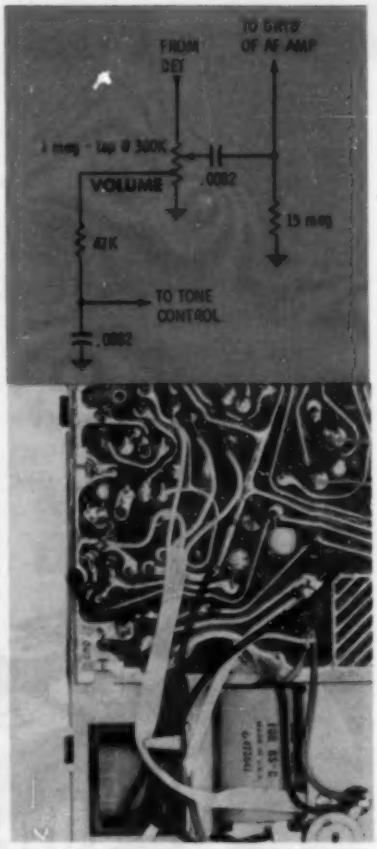

Fig. 2. Whistle in a Model 75BF was traced to the volume control circuit.

Whistle While You Work

One 75BF we had in the shop emitted a piercing, strange-sounding whistle. Probing around on the wiring side of the printed board caused this noise to occur intermittently. We finally traced the trouble to the volume-control circuit (Fig. 2A). In this set, the volume control is connected to the printed wiring by the white, flat, four-conductor cable shown in Fig. 2B, which is soldered to appropriate places on the board. Careful manipulation of this cable indicated that one of its conductors was broken—apparently the ground lead. We did not suspect this fault at first, because the insulation at the end of the wire had become melted and mixed with the solder at the connection—thus giving a firm mechanical connection when it again solidified, and defying our first tugs in attempts to find a loose wire.

Stations Few

Troubled with weak reception of

local stations in these '57 Ford radios, and no reception at all on weaker stations? Maybe the trouble is the same one we have been having—an open coil in the plate circuit of the RF amplifier (Fig. 3). Since this coil is shunted by a fairly low-value resistor, the stage still seems to function—but sensitivity is not what it should be. Another possible cause for the trouble is an open RF cathode resistor, part of a component-combination unit.

Speak Up!

Here's one case that wasn't the fault of the radio at all. The lack of volume in one of the 74BF's under our care was a real puzzler. The transistor had been replaced, necessary bias adjustments had been made, IF and RF sections had been realigned, tubes had been checked and replaced if they were at all weak—yet the maximum output wasn't enough to rattle the speaker. Although the sound was loud enough for ordinary circumstances, it wasn't adequate for conditions of rolled-down windows and high speeds. Besides, other radios of the same type had much more volume.

A casual glance at the speaker, when the radio was out of the car, revealed that a standard 6″ x 9″ oval unit was being used. Just on the chance that the speaker might be the problem, the service literature was consulted with the idea of obtaining a recommended replacement. The lack of any listing other than the original Bendix part number made us wonder if perhaps the

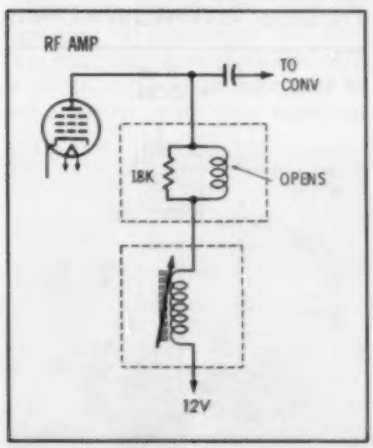

Fig. 3. Several cases of weak reception were traced to open RF plate coil.

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speaker was a special unit. When the original type was installed, the volume level returned to normal. Further checks revealed that somehow a 6-8 ohm unit had been installed instead of the required 3-4 ohm unit. Mounting requirements and space considerations probably had a lot to do with the choice of an improper unit.

Beat on Dash for More Volume

This auto-radio trouble symptom is characteristic of tube or transistor defects, so the problem was not at first considered serious when it occurred in one 74BF. When substitution of tubes and the output transistor failed to improve reception, however, all sorts of reasons began to come to mind — cracks in the printed board, a defect in an IF can, a bad volume control, a bad tube socket, etc. Hoping for the best, though, I started a careful visual analysis of the wiring board. A strong light was employed, and every connection was carefully inspected. When the area occupied by C2, R2, and R15 was scrutinized (Fig. 4), a long "whisker" was noted on the C2 end of R15. It seemed to be dangerously near the metal chassis. A little pulling and tugging on C2 quickly convinced me that this was the "brute-force volume reducer."

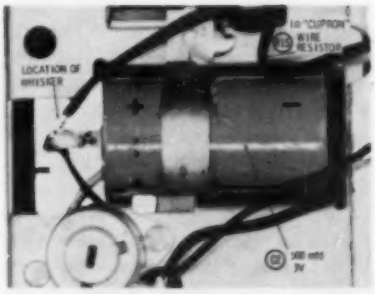

Fig. 4. Wire stub shorting to chassis caused intermittent volume changes.

When the whisker had been removed, the set was given an operational check. The intermittent condition was gone, but the volume still wasn't up to par. A complete IF alignment helped, but it didn't produce entirely satisfactory results. The dummy antenna recommended for RF alignment was next constructed by attaching a 30-mmf capacitor from the antenna input to chassis and another between the antenna input and the hot lead of the signal generator. Adjustment of the oscillator, RF, and antenna trimmers, using the recommended procedure, brought the volume up still further. It was at this point that I noticed and began to wonder what to do about the SENSITIVITY control (Fig. 5). No adjustment procedure could be found for it. However, after studying the circuitry a few minutes, I decided that this control provided an adjustable bias voltage for the cathode of the RF stage. The control was obviously not likely

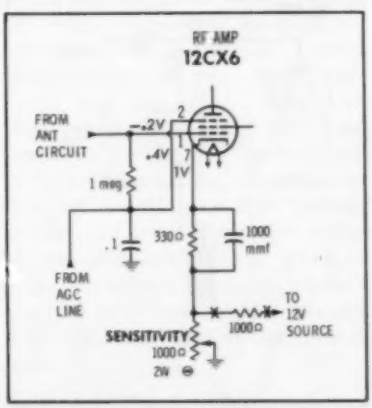

Fig. 5. Sensitivity control adjusts the cathode bias of the RF amplifier stage.

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to cause any trouble through burnout of components if misadjusted (as is sometimes the case with controls in transistorized output circuits); therefore, it was rotated throughout its range. The volume varied from very weak at one extreme to strong and distorted at the other. Reasoning that the control's action was similar to that of the AVC circuit, I proceeded to tune in the strongest local station (with test-bench antenna fully extended) and adjusted the control for maximum undistorted volume.

The net result of these operations was a repaired radio and a satisfied customer. However, this job caused me to think about the number of times I had aligned a radio IF without a touch-up of the oscillator, RF, or antenna trimmer, and made me wonder how many of these sets would have worked better if I had just taken the time. As you well know, each signal generator is just a little bit different and has a slightly different frequency-tracking characteristic. This means that retuning an IF without retracking the antenna, RF and oscillator stages can result in a slight case of misalignment caused by alignment!

One further hint: Using the two 30-mmf capacitors for a dummy antenna during RF, oscillator and antenna trimmer alignment eliminated the need to readjust the antenna trimmer with the radio installed in the car.

CRT Brighteners

At one time, selecting a picture-tube brightener was a simple matter —there was only one type. Also, the usefulness of brighteners was limited, since they were applicable only to picture tubes which were good in every respect other than emission.

Today, the story is much different. Modern CRT heaters have six different voltage ratings and five different current ratings. Brightener manufacturers have kept pace, and are producing a wide range of units to meet the various needs.

Perma-Power's *TV Tube Restorer* is a good example of a unit which does more than increase cathode emission. Designed for use with standard tubes having 6.3-volt, 600-ma filaments, it can be used in either a series or parallel filament circuit. Furthermore, it provides a connection which permits selection of either normal or boosted heater voltage. Other design features make it possible to restore operation in tubes suffering from open cathodes, heater-cathode leakage, and even grid-cathode shorts—a far cry from boosting emission only!

By the way, Perma-Power has recently produced a handy leaflet entitled, "Guide to Proper Britener Selection," which includes a "Quick Selector Chart" that shows the proper type of brightener to be used with each type of picture tube.

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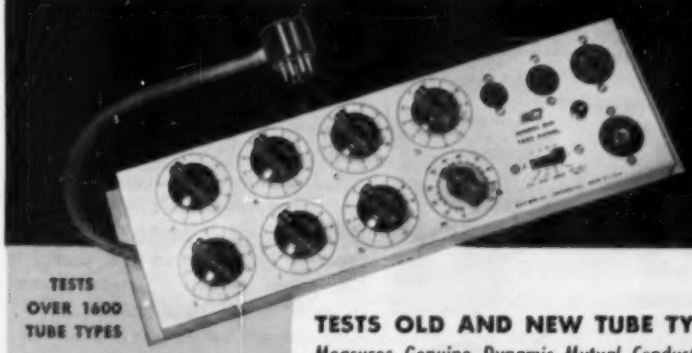

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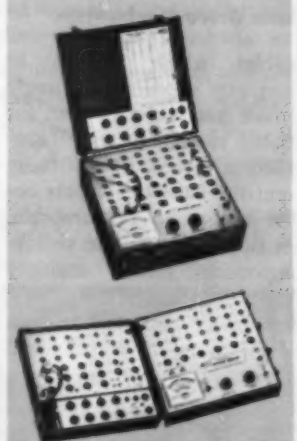

Photos above show how easily the new Model 610 Test Panel fits into the B&K Models 550 and 650 Dyna-Quik Tube Testers.

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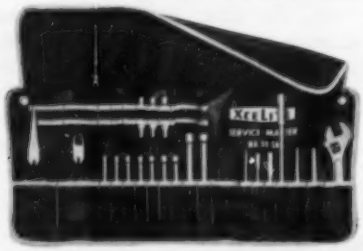

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AUDIO FACTS
BY ALAN ANDREWS

speed problems with phonos

One of the most prevalent problems you are apt to be faced with when servicing phonos is that of speed. Most often these problems fall into three general groupings: The turntable does not rotate at all; it turns too slowly; or the speed varies depending upon operating conditions. As might be expected, the more expensive types are usually less afflicted with speed problems than their less expensive counterparts. Also, as a rule, turntables designed to operate at only one speed, and those not involving a changer mechanism, have fewer speed problems than the three or four-speed record changers found in most home installations.

Basic Drive Mechanism

Turntables which operate at more than one speed use a single motor which has the same rpm for all available record speeds. Turntable speed is varied by switching in different-sized drive elements between the motor and the turntable. And, not surprisingly, these switching components greatly multiply the speed problems.

While phonos employ various types of drives, such as gear and belt, most home changers use a system like one of those shown in Fig. 1. The one in part A is a three-speed turret-type drive, with three idler pulleys on a single mount, and was widely used in earlier three-speed phonos. The system in part B differs from A in that the drive pulleys are mounted directly on the motor shaft. (Notice the four steps common to today's four-speed phonos.) Except for other minor variations involving the mechanics of shifting from one pulley size to another, the principles of the two arrangements are pretty much the same. Both are referred to as rim-drive systems because the turntable is driven by force applied to the inside of the rim. In operation, the motor shaft turns the active idler pulley which, in turn, drives the idler wheel and thereby rotates the turntable. A rubber tire surrounds the outer diameter of the idler wheel to increase traction between it and the smooth metal surface of the turntable rim.

Fig. 2 is a side view of a portion of the rim-drive arrangement. This drawing shows how the various drive elements are situated with respect to each other, and how each in turn drives the next section.

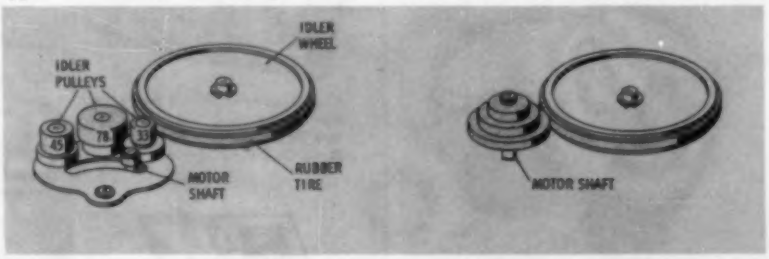

Fig. 1. Two types of rim-drive systems often used in home record changers.

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Rotating the turntable by hand will give an indication of whether any part of the changer is jammed or excessively loaded in any way. In some cases the mechanism may be freed by rotating the turntable in the reverse direction. Recycling by hand, while observing the operation, may reveal the cause of jamming or binding. This condition is most often caused by accumulation of grease and dirt, bent parts, and burred or excessively worn moving parts. Cleaning with alcohol, carbon tet, or a similar solvent, will remove all foreign matter. Bending or filing parts of the changer mechanism may be necessary in some cases. Parts which are worn excessively should be replaced to effect a more permanent repair.

If the changer mechanism is not binding in any way, the lack of rotation could be caused by a motor defect. First, check to see if the idler wheel and pulley are making contact as they should. Usually, poor contact in these areas only

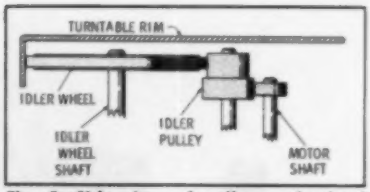

Fig. 2. Side view of pulley and wheel arrangement for turret drive system.

slows the speed, but these parts should be checked anyway. Next, try to turn the motor rotor by hand.

If the rotor cannot be easily turned, check the spacing between the stator and rotor through a complete revolution. If necessary, the rotor can sometimes be realigned by loosening the end plates and tapping the shaft very lightly until alignment is correct. Then tighten the screws so that the end plates remain in correct position. Worn bearings may also cause uneven alignment between motor and stator. In this case, replacement of the entire motor is easier and less time-consuming than replacement of the bearings.

Other conditions which hamper rotation of the motor are hardened grease and dirt, tight bearings, dust accumulation, and rust. Disassembling the motor and cleaning its parts with a solvent may remedy the situation. Polishing the rusted metal parts with crocus cloth may also result in some improvement. When lubricating the motor use only a high grade of motor oil; SAE 10 is about the right weight. *And use the oil sparingly!* In record changers, excess oil almost always causes trouble sooner or later. For lubricating cams, gears, and sliding parts, a thin coat of *Lubriplate*, or equivalent, is recommended.

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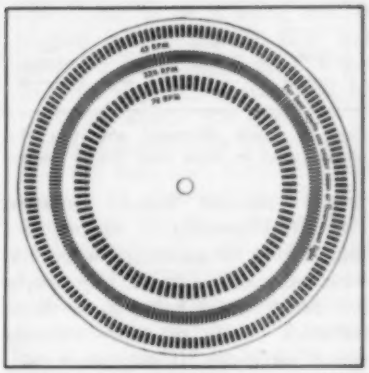

Fig. 3. Sample of strobe disc used for checking variations in turntable speeds.

electrical. Assuming that the switch and connecting wires are all right, the trouble possibilities include opens or shorts within the windings, or shorts to ground. An open circuit in the motor usually results in no rotation at all. Shorts in the stator coils cause overheating and decreased turning force. Here again, it usually is better for the average technician to replace the entire motor rather than attempt to repair it.

Slow Speed

Slow or erratic speed can be caused by some of the same faults which produce complete loss of rotation. In these cases, the trouble has not yet reached the stage where operation is halted altogether. Repairs, in many cases, are similar to those mentioned previously.

In the synchronous motors used in record players, basic speed is determined primarily by the frequency (60 cps) of the supply line. It is unusual to encounter a condition where the speed is too fast (except slightly so). Excessively slow rotation is much more common, usually because of slippage between the motor shaft and the turntable itself, or because of gummy motor and drive assemblies.

Ordinarily, the idler wheel is positioned in a slot and held against the turntable rim by a spring. A loss of tension in this spring is a possible cause of slippage between wheel and turntable. It is better to install a new spring than to try cutting off a section of the old one, since the latter remedy sometimes increases turntable rumble by reducing damping of the unit.

Gradual accumulation of oily substances on any of the drive elements causes them to lose traction, with a resulting decrease in turntable speed. Cleaning the various parts with alcohol or a special cleaner designed for this purpose will clear up the condition. Carbon tet is not too good for cleaning rubber parts because it acts as a solvent; many such cleanings may make the rubber gummy. Drive-element surfaces which have become slick can be coated with a special non-slip chemical to provide better traction.

Again, lubricate as little as possible, consistent with good operation. Immediately wipe off any excess oil because it will only cause trouble later on. Any rubber drive components which have become hard or glazed should be replaced because they are beyond repair. The entire idler wheel could be replaced, or only the rubber tire which surrounds it. Assortments of these tires are available from most parts distributors.

Wow and Flutter

Actually, a slight error in turntable speed is not very objectionable to most listeners as long as the speed

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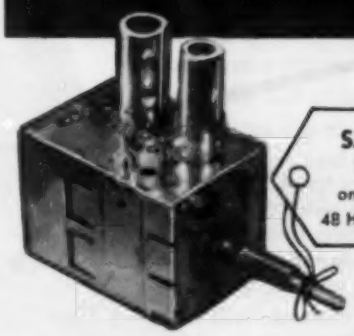

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is constant. Much more annoying is the condition where the speed continually changes. When these changes occur at a relatively slow rate, the condition is called "wow"; when they occur at a faster rate, the term "flutter" is used.

Before attempting to track down the cause of the speed variations, make sure the fault is not in the record. Center holes which are too large, warped discs, or poor recordings can all cause unwanted speed variations. Does the trouble occur for all records or just for certain ones? Does the trouble occur on all speeds or on just one? Is there any difference in reproduction when several records are stacked on the changer? The answers to these questions sometimes point the way to a solution of the trouble.

Slippage between drive components sometimes produces random speed variations which occur in no set pattern. This slippage may be caused by too little tension on the drive elements, accumulation of oil or grease, or hard or broken rubber on the drive elements. These troubles can usually be cured by cleaning the drive components so that proper traction occurs between them. Replacement of various elements may be necessary when the wear has been excessive. Improperly lubricated motor bearings or drive elements also produce random speed variations. It may seem odd, but in the case of wow, too little lubrication can cause the same effects as too much.

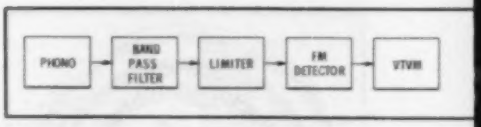

Fig. 4. Block diagram showing the stages used in wow and flutter meter.

One test for slippage is to touch the rim of the turntable while it is in motion. It should slow down to some extent, but the pull should remain constant throughout each revolution. Any slippage can be felt with the finger.

Indentations or breaks in the idler wheel rubber can cause rhythmic variations in speed. That is, the fluctuations occur at a regular rate for each turntable speed, and are more noticeable for the slowest speed (usually 33⅓ or 16⅔ rpm). Installing a new idler wheel or new rubber tire is the only cure. As a note of advice for the user, urge him to set the speed control to "off," thus disconnecting the drive wheels from each other. Leaving the turntable on the same speed setting for long periods of time when the player is not in use very often leaves a flat spot on the idler-wheel tire. A similar type of wow could be produced if the turntable rim were accidentally dented by being dropped or struck a hard blow.

Measurements

Turntable speed can be checked by using a stroboscope disc of the type shown in Fig. 3. Most often made of cardboard, it is imprinted with several rings of dots or bars. It is placed on the turntable in the same manner as a record, and with the mechanism in motion, the dots are observed under a light energized from a 60-cps source. A neon or fluorescent lamp is best.

As an example, let's assume we are checking the 33⅓-rpm speed. The middle ring of dots would be used on the disc of Fig. 3. If the speed is correct, the dots in this ring

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will appear to be standing still. If rotation is too fast, the dots will move in a clockwise direction; if too slow, the apparent motion will be counterclockwise. The presence of wow is indicated when the dots seem to move back and forth. Slippage can also be observed by using the strobe disc. In this case the dots would alternately stand still and move counterclockwise.

While speed variations can also be checked by playing a test recording of a steady tone at some frequency, this method is not too practical because it requires comparison of the reproduced note with some known frequency standard.

A strobe disc can also help to determine if turntable speed varies with line voltage. By using a variac with a range of about 105 to 125 volts to supply AC input to the phono motor, the strobe disc can be observed to see whether or not there are unwanted variations.

The extent of wow and flutter can be measured using a "wow and flutter meter," a block diagram of which is shown in Fig. 4. Speed changes cause variations in pitch, so they really frequency-modulate the signal. Thus, the basic method of measuring speed changes is to measure the FM which is produced when the phono is operated.

To make the measurement, a steady sine-wave signal is supplied by a test record. The most commonly used signal frequency is 3,000 cps. Inside the meter, this signal is fed to a bandpass filter which eliminates everything except the test frequency and a small band on both sides. Amplitude variations are then eliminated by a limiter (clipper) circuit, after which the signal is applied to a discriminator that converts the FM caused by wow into amplitude variations. This detector circuit is very similar to that used in FM radio receivers.

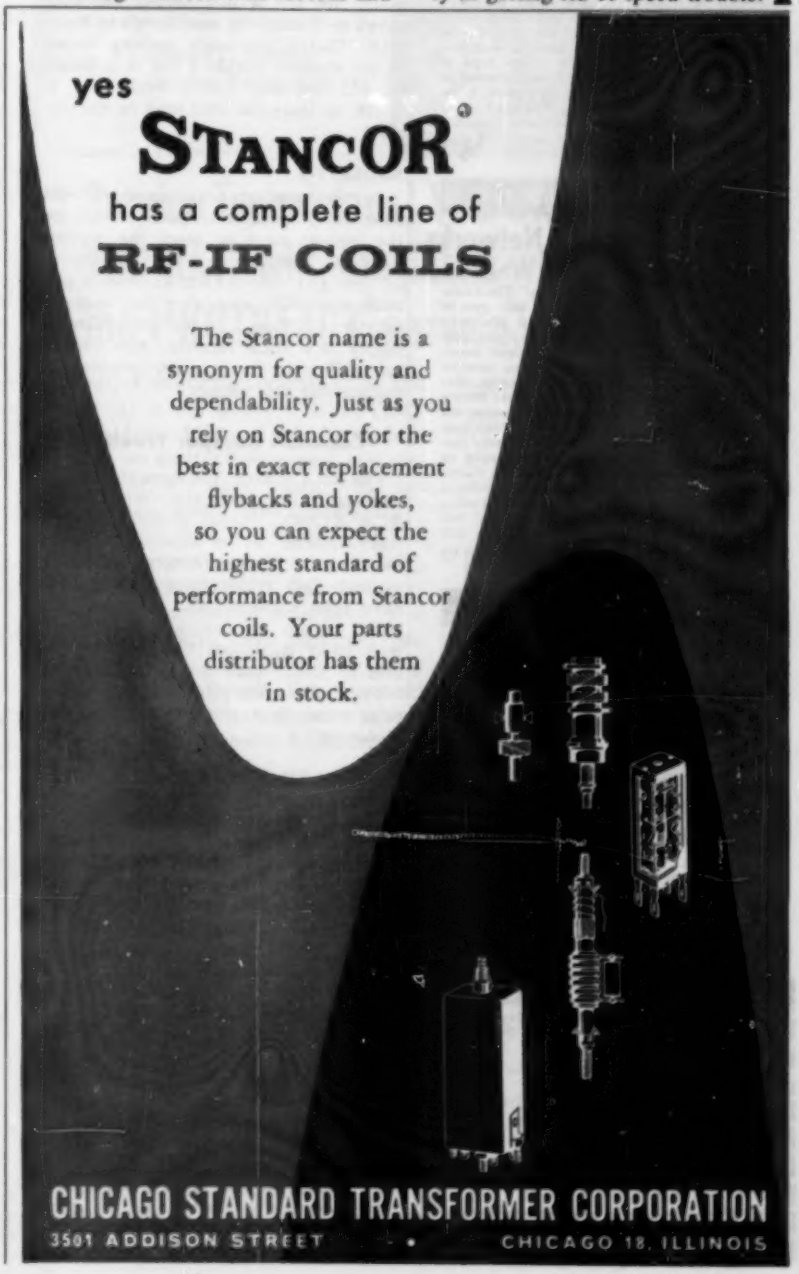
The output voltage of the discriminator is applied to the VTVM circuit in the instrument. The meter scale is calibrated in "percent of flutter," which can be defined by:

$$\% \text{ flutter} = \frac{\text{max. freq.} - \text{min. freq.}}{\text{avg. freq.}} \times 100$$

The average frequency is that which is applied to the system (3,000 cps as mentioned). The maximum frequency minus the minimum frequency represents the total frequency change. If there is no frequency variation, there is no output from the FM detector, and the meter reading is zero. As speed changes become more pronounced, there is greater detector output, and a higher meter reading. A reading of 1% or less is acceptable for a turntable; some of the better-quality units may produce readings as low as 0.1%.

Measurements made under actual playing conditions are of more value than any others. Therefore, the measurements should be made with the changer loaded with records and with the stylus on a record. In this way any drag produced is more noticeable. Also, by checking a unit both with and without a full record load, it can be determined whether or not the load has any effect on the speed.

Every phono model is different from all others, so no general servicing procedure can be expected to apply in all details of every case. Careful and thoughtful observation of the unit being repaired, plus reference to the instruction manual for that particular player, can aid greatly in getting rid of speed trouble. ▲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Advisable Change

A Philco color chassis TV-123 keeps blowing the #26 fuse wire protecting the filaments. In checking the current on this line, I find it surges to 27 amps when the set is first turned on, then drops to 8 amps (its rated level) in 8 seconds. There's absolutely nothing wrong in the filament circuit. I put in a length of #22 fuse wire and it works fine. Is it OK to leave the #22 wire in the circuit?

E. J. CAROLAN

Natalia, Tex.

In the case of color receivers with their many tubes, it is quite normal for the current surge to reach the proportions you indicate, and for the interval of time you report. Field experience dictates that #26 wire does not make a satisfactory fuse line for the filament supply in a color receiver. New chassis use #22 wire, so you are justified in making this field change.

Common Damper Troubles

I've got a stinker. The damper-filament winding of the power transformer in an RCA KCS47C chassis shorted out and was replaced by a separate filament transformer. This arrangement hasn't worked; two replacement transformers have been knocked out. I've been advised to use an isolation transformer with 10-kv insulation, but haven't been able to locate such a unit at any distributor. Can you please suggest something other than power-transformer replacement?

BEWILDERED

Advanced TV Service Center
Amsterdam, N. Y.

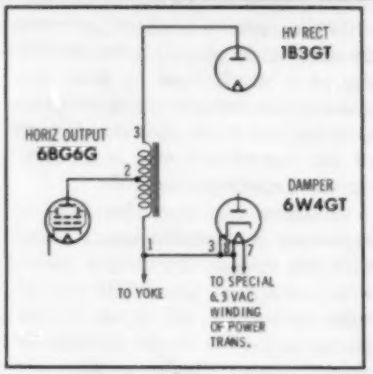
The damper-tube filament and cathode are wired together in a Capehart Model 323M. This has caused the filament winding to short to ground. Is there any way to get around replacing the power transformer?

JOHN GALLO

Brooklyn, N. Y.

Both of you have encountered the same trouble in almost identical circuits. The direct-drive horizontal sweep circuit in these receivers was designed when the 6W4 was about the only damper available. In view of the relatively low peak heater-to-cathode voltage rating of the 6W4, it was necessary to connect heater and cathode and use the specially insulated winding of the power transformer.

The solution to your problem is quite simple. Just remove the wire connecting the cathode and filament, leave the flyback connected to the cathode, use a regular filament transformer (with 2500-volt insulation) of the correct current rating to feed all tube filaments in the set, and replace the 6W4 with a 6AX4GTB. The higher heater-cathode voltage rating of this improved tube design will solve the problem for you.



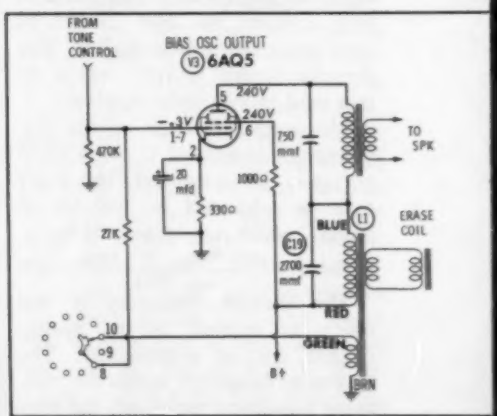
Won't Erase

I'm having trouble finding out why a Federal Model 37-B tape recorder won't erase. All voltages agree with those shown in PHOTOFACT Folder 259-6. The head has been replaced and aligned, and the selector switch has also been changed.

PAUL A. KALUZNE

Savannah, Ga.

Connect a scope across the erase coil to see if you have any signal. If you do, be sure the pressure pad is holding the tape in firm contact with the head. If no signal is present, or if it's extremely low in amplitude, see if there is a greater signal amplitude at the transformer secondary; it may be advisable to disconnect the leads in making this test to be



sure the signal is not being shorted by the connecting cable. If there is still no signal, substitute for C19; be sure the bias-oscillator feedback signal from the green lead of L1 has a continuity path to the control grid of V3. If there is still no erase signal, bias-oscillator coil L1 is probably the culprit.

Silicon Score

Looking through some back issues of PF REPORTER, I noticed the "Troubleshooter" recommending to Mr. R. E. Rumpf (March, 1960) that he use a 7.5-ohm resistor when converting from selenium rectifiers to silicons. Does this hold true in every case? If not, what do you use where?

ARTHUR DOEHNERT

Houston, Tex.

The required value of series resistance used in conjunction with selenium, silicon, or germanium rectifiers depends primarily on two things: (1) the circuit configuration; (2) the specific rating of the rectifier itself. Each rectifier has certain specifications; one is the minimum value of the limiting resistor. This is normally around 4.7 ohms for silicon units; however, typical operating conditions usually call for a value somewhat above the minimum standard. Since silicons have a much lower forward resistance than seleniums, conversions normally require an increase in value for the series-limiting resistor to provide surge protection for the rectifiers. More or less standardized values are as follows: For a half-wave circuit, 6.8 ohms; for both half- and full-wave doubler circuits, 7.5 ohms. In making conversions, it's a good policy to experiment with different values until you find the one that produces the normal B+ of the receiver.

Like a Sponge

I'm fully aware that rain and snow affect television signal strength. However, I've been told that reception varies according to whether or not trees have their leaves. Is this true? I don't remember ever seeing an explanation of either phenomenon — can you fill me in on the "why"?

KENNETH E. CRAWFORD

South Covington, Va.

You're so right! Trees, snow, rain, etc., all have a pronounced effect on a TV signal. For that matter, anything and everything the signal may encounter between the transmitting antenna and the receiving antenna absorbs a certain amount of the transmitted energy, just as a sponge soaks up so much water. The amount of signal attenuation varies with the material, weather, etc. Another rather important factor is the area of the material. For example, a tree with leaves will absorb considerably more energy than one with no leaves. Also, both snow and rain attenuate the signal by providing a leakage path to ground. Normally, such losses are not even noticed in strong-signal areas. However, under fringe or weak-signal conditions, they may have a pronounced bearing on reception.

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TV Radiation Hazard

(Continued from page 27)

tion, this instrument features a completely transistorized spectrometer circuit which supplies all the necessary signals to activate the graphic recorder also pictured in Fig. 2.

The *slave scaler* is a digital computer with a highly accurate built-in timer and mechanical register. Through its use, the radiation count may be tabulated for certain preselected time cycles. This unit also receives its controlling impulses from the linear count ratemeter. Although not used during our low-level experiments, the *well shield* is also a component part of the entire Spectrometer System. When "hot" radioactive materials are under analysis, they are placed in this isolation chamber.

Some of the others items of equipment assembled for our X-ray tests were a special mechanical arm for securing the detector probe, an accurate high-voltage meter, a variable AC power supply, and, of course, a number of television receivers. (See Fig. 3.) Since the major factor governing the amount of radiation is accelerating potential, we chose only those TV chassis that developed normal anode voltages in excess of 16 kv for our principal guinea pigs. This involved popular brands with both 21" and the newer 23" screens.

Test Results

The task of performing accurate radiation measurements is not as simple as taking voltage readings or checking TV waveforms. Aside from the highly specialized equipment re-

"Yoo hoo. Sorry to bother you on your day off"

quired, the receiver's operating conditions had to remain constant, the detector system had to be calibrated or zeroed continually to compensate for background readings, and the sampling probe had to be held absolutely rigid for given time intervals. We also had to make certain that light and stray magnetic or electrostatic fields did not upset our readings.

The first few tests we performed were on sets operating with normal rasters, high voltages from 16 to 19 kv, and no picture modulation on the screen. After sampling all surface areas of the picture tubes, we found an almost unmeasurable amount of X-ray radiation. For all practical purposes, the radiation detected even at maximum points was at a rate of considerably less than 1 mr per hour.

We also investigated the possibility of radiation from the neck of the CRT, and in or around the high-voltage compartment. Our findings here were nil; if there was any radiation present, it was certainly less intense than that slight amount detected on the larger surfaces of the picture tube.

In our next series of tests, we performed various readouts with the receivers "bugged" to simulate a number of abnormal operating conditions that could very well prevail at the service bench. Brightness and sweep controls were all varied, centering misadjusted, vertical sweep collapsed, high voltage varied, and ion traps moved to different positions. Radiation readings were relatively unchanged except for one certain set of conditions.

With receiver brightness above a normal viewing level, high voltage in the vicinity of 20 kv, and the vertical sweep collapsed, we detected a radiation peak at several locations on the back side of the picture tube bulb. (Two of the four "hot spots" are illustrated in Fig. 4.) The radiation count was considerably higher under these conditions and at these particular points, but still in the vicinity of 1 mr/hr even though the probe was as close to the source as possible.

Under the same conditions of no vertical sweep, we did detect a few spots on the front of the TV screen where the count approached 1 mr/hr. Much to our surprise, however,

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it was not in the center of the screen where the beam was concentrated, but near the corners (Fig. 5).

Singling out one of the receivers with which we could obtain an anode voltage of about 23.5 kv, we ran a complete spectrum analysis of the radiated X rays, using the graphic recorder pointed out in Fig. 2. While monitoring the X-ray radiation, the spectrometer system scans a predetermined energy range and graphically records at what precise levels the energy peaks occur. For our experiments, a scanning range of from approximately 1 kev to 100 kev was selected. Higher ranges were also scanned, but no peak radiation was indicated.

The graph shown in Fig. 6 represents the results of our spectrum analysis. Once we obtained an energy peak from the TV X rays, we needed an accurate way of determining the energy level at which the peak occurred. This was a simple task for the radiation specialist; he merely selected a low-level radiation substance of known activity and superimposed its energy peaks on the original graph. The substance used for this calibration was "lead 210,"

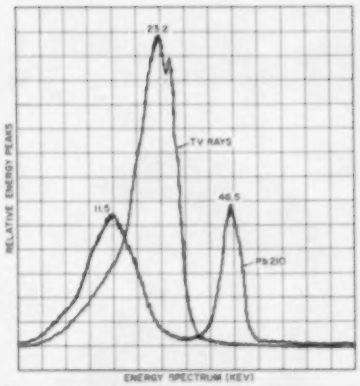

Fig. 6. Spectogram showing the energy peaks of TV radiation and "lead 210."

which exhibits energy peaks at both 11.5 and 46.5 kev. As can be seen in Fig. 6, the two calibration peaks straddled the TV radiation curve and thus gave us a means by which to interpolate the energy value noted.

We also ran spectrometer tests at slightly lower accelerating-anode potentials. Here, we came up with energy peaks at 22, 20.6, and 19.4 kev. We noticed, however, that they were a little lower in magnitude than on our original run. It was interesting to note, too, how settings of the receiver's brightness control affected the radiation count. When a brightness control is advanced, beam current increases but high voltage decreases. We found, therefore, that peak radiation did not occur at either maximum brightness or maximum high voltage, but at an in-between point where voltage was relatively high, yet there was adequate beam current to bombard the screen.

Summarizing the results of our tests, we found no measurable quantity of radiation in receivers operating with anode potentials of less than 16 kv. On large-screen receivers with higher potentials, we found that only the CRT itself offered emitting surfaces, and no radiation of any significance was detected on any other portion of the TV chassis.

TV Radiation and You

Undue exposure to X-ray radiation has been known to affect the well-being of both humans and animals. Some of the obscure biological effects caused by large doses of radiation are malignant tumors, impaired fertility, cataract, obesity, and

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over-all reduction in life span—not to mention the total genetic effects which have yet to be determined. Milder doses of radiation have been known to lead to various degrees of skin burns, leukopenia, low blood pressure, and anemia. These, of course, are only a few of the reasons why we concern ourselves with this energy that we can neither see or feel.

Now for the paramount question: What is a permissible limit of radiation dosage? One widely-accepted recommendation (by National Committee on Radiation Protection quoted in *National Bureau of Standards Handbook 59*) states that, for long-term exposure of the whole body to X rays for an indefinite period of years, the basic permissible dose should not exceed 300 mr per week in the blood-forming organs—considered the most critical tissue in the body.

The NCRP has defined a permissible weekly dose as "a dose of ionizing radiation accumulated in one week, of such magnitude that, in the light of present knowledge, exposure at this weekly rate for an indefinite period of time is not expected to cause appreciable bodily injury to a person at any time during his lifetime."

Although absolute limitations on radiation exposure cannot be stated at this time, we concluded from our tests and medical references that even if a technician or serviceman remained in direct contact with a radiating picture tube for 40 hours a week, the dose received would still be extremely unlikely to exceed the present-day safety ratings. Another encouraging point is that radiation intensity is inversely proportional to

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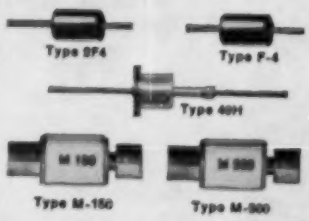

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the square of the distance from source to object; for example, if we had simply moved our detector probe back about 6" from any given spot on the tube's glass, the radiation intensity would have been approximately ¼ that previously obtained.

Thus, as far as present-day TV receivers are concerned, there is no real reason for alarm, especially when you take into consideration the following points:

1. Only certain TV receivers operating under abnormal conditions produce enough radiation to be actually recorded, even with measurements made as close to the radiation source as is physically possible.
2. The relatively soft X rays produced by a TV set would have a difficult time even penetrating the outer layers of the skin.
3. X rays can be entirely blocked or reduced in intensity by the shielding effects of objects such as a metal chassis or safety glass.
4. The average close-range exposure time is usually only a small fraction of the maximum periods considered. (One seldom rests his hand habitually on the back of an operating CRT!)

What does all this prove? Simply that the X-ray radiation detected during our experiments could very well be classed in the same category as that produced by the luminous dial of a wrist watch—something we live with every day. ▲

"Don't get so upset. I just asked if you wanted a cup of coffee."

Admiral 21F1

(Continued from page 24)

plate voltage of V7 would also appear on the cathode of the CRT. On the other hand, if R37 opened, the DC voltage would not reach the cathode. Then, due to insufficient bias, the brightness control would fail to cut the CRT off.

Measurement of C26 revealed some leakage, and a resistance check of R38 (a half-watt resistor) showed this component to be wide open. With more than 200 volts applied to the cathode, and never more than 125 volts on the grid, the picture tube was driven well into cutoff —an excellent reason for the lack of a raster! Replacing C26 with a 0.1-mfd, 600-volt molded capacitor and R38 with a new 560K-ohm, 1-watt resistor brought back a picture, of sorts, with a fair amount of contrast and brightness. But a lot of work was still necessary before the set was restored to the pink of condition.

I started by checking all tubes and cleaning that decrepit tuner. Then I decided to try increasing the boost and high voltage, in hope of brightening the picture. The DC voltage on the boost line measured 370 volts, not quite 10% below the stated value of 400 volts. The B+ voltage itself was a bit low (280 volts DC, instead of 300), but the low voltage supply circuit was otherwise normal. Checking the boost circuit (Fig. 2), I found that C61 was OK, but C62 through C64 were leaky—and C65 (in series with the low side of the yoke) was almost shorted. After I finished replacing

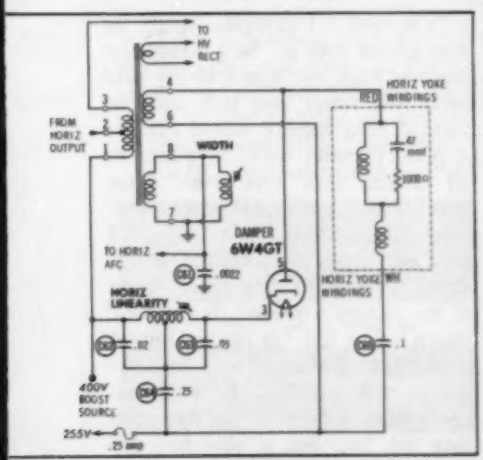

Fig. 2. Horizontal sweep and boost circuits used in the Admiral Model 21F1.

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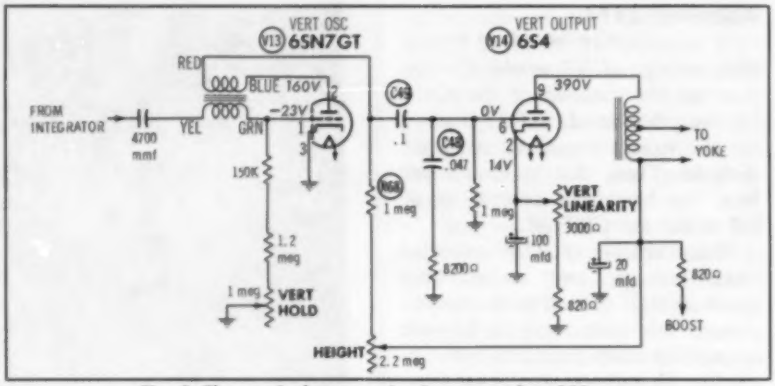

Fig. 3. The vertical sweep circuit operated at 120 cps.

these parts, the boost voltage rose only about 5 volts. However, the time hadn't been wasted, because the raster and picture were noticeably improved. By the way—these capacitors, plus a new 1B3, raised the high voltage to 11.5 kv. I figured this was good enough, considering the age of the set. Even so, my friend and I still had plenty of trouble on our hands.

Poor Joe

What the Sam Hill was wrong with the picture now? The bottom had pulled up several inches into a white fold, and there were heavy retrace lines across the screen that wouldn't come out at any combination of brightness and contrast settings. By this time, the old 21F1 had exceeded my worst expectations. To put it mildly, the set was a mess! Poor Joe; over an hour had already gone by, and there he sat patiently waiting. "Friend," I said, with a sigh of resignation, "don't you think you'd better leave this and come see me another time?" He nodded in mute agreement and departed — disappointed, I suppose, that I wasn't the perfect miracle man after all. For my part, I turned the set off, went over to the coffee urn, poured a generous portion of the blackest, and strolled about the shop considering whether or not to call it quits. If ever a set needed repairing, this one certainly did. I figured I was going to earn every cent of my labor fee this time—and definitely the hard way.

Rock 'N' Roll

"Oh, well," I thought, "might as well get on with it." So I turned the receiver back on. Much to my surprise, the raster was full, and the vertical hold control would execute a perfect center lock. In addition, all retrace lines were gone. I sat dumfounded; such things could happen, I'd heard, but why to me? I was just about to grab the phone and call friend Joe when the bottom of the picture whitened, curled, and began a slow roll. "A vertical output tube will fix this in a hurry," I jubilantly told myself, knowing that 6S4's have a habit of failing when they get hot. But a new 6S4 did absolutely nothing to remedy the situation. The picture began to roll

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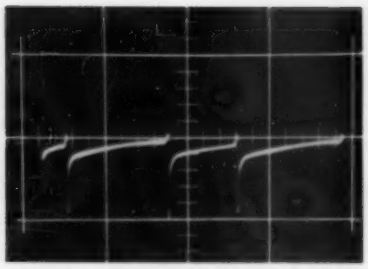


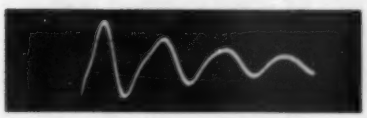
Fig. 4. Grid waveform of oscillator revealed increase in sweep frequency.

even faster, and I could almost feel my eyes clicking like pool balls. I was well behind No. 8 on this one.

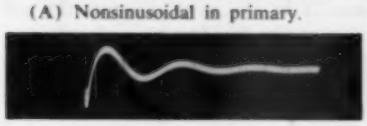
I began concentrating on the vertical sweep circuit (Fig. 3). With the scope-sweep frequency still set at 30 cps, I checked the grid waveform of the vertical oscillator. The pattern locked in fairly easily (see Fig. 4), but I was surprised to see that the oscillator was running at double the normal frequency. In addition, the waveform was composed of alternate long and short cycles. Puzzled, I took another glance at the picture. There appeared to be a single image, but the raster fell far short of filling the screen vertically. The retrace lines were more pronounced than ever.

Resistance checks across the vertical hold control and its series resistors showed nothing unusual. The height control and R68 were also well within tolerance. Both C48 and C49 showed a little leakage, but substituting new units failed to change the symptoms. Since the remaining components were not immediately in the circuit being explored, they were ignored for the time being. I decided to take a chance on substituting another new 6SN7 for the vertical oscillator, but as I suspected, this didn't do a bit of good. What else was left? Just what I had avoided tackling all along—the blocking-oscillator transformer.

The DC resistance readings across



(A) Nonsinusoidal in primary.



(B) Overly-damped in secondary.

Fig. 5. Pulse test of transformer produced a pair of abnormal waveforms.

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the primary and secondary windings tallied almost exactly with the values given in the sweep-transformer parts list. However, I wasn't too impressed with this finding, since I knew that the trouble had not been evident when the set was first turned on. I still suspected the transformer, even though the "cold check" with the ohmmeter had failed to turn up any trouble; thus, I felt that a more conclusive test was needed. Since I had some blocking transformers in stock, I decided to see if a substitution check was possible.

Checking the replacement-unit numbers given in PHOTOFACT Folder 135-2, I was pleased to find that a transformer in my stock was electrically similar to one of these replacements. Since both the secondary and primary leads of the old transformer were already disconnected, I connected my spare into the circuit with some hook-up wire and alligator clips I keep handy for such occasions. When I turned the receiver on again, everything worked fine; even the height and linearity controls could be adjusted without producing picture flipping. Neither was there any vertical foldover. With a silent prayer, I walked away from the set and helped myself to another large mug of black coffee. As the receiver "cooked," I steadily became more cheerful. After 20 minutes, there still was neither flip nor fold. Evidently another transformer was the ticket to this repair.

Now to select the new part. Original specifications called for Admiral transformer 79A18-2, but I noted that the defective unit carried the number 79A18-4. This version called for a slightly different replacement, according to the local distributor from whom I ordered the new part.

—and Double Check

The new unit turned out to have a different DC primary resistance from the 79A18-2, so the supposedly "good" resistance reading on the old transformer actually would have pointed to trouble—if I'd only known. It's a good thing I didn't take the resistance check too seriously.

Suppose my stock hadn't included a suitable transformer for the substitution check—could I still have found the trouble? The answer is yes, because it so happens that I've wired a 680-mmf capacitor from the cathode of my oscilloscope's time-base sweep oscillator to a jack on the front panel for occasions just like this. With the pulse voltage thus obtained, I can check the condition of most TV transformers in-circuit as well as out. Connecting a jumper from this special scope jack to one primary lead of the old blocking transformer, and hooking the vertical input terminal of the scope through a direct probe to the other primary lead, I obtained the top waveform in Fig. 5. Notice that the ringing produced by the scope pulse is not in the form of a pure sine wave. Also notice the highly-damped waveshape on the secondary (lower waveform in Fig. 5). Now look at Fig. 6, produced by applying the sweep pulse to the primary and secondary coils of the new transformer. It's easy to tell which is the good one, isn't it? The same test can be made on some units in-circuit, but it would have been much more difficult to evaluate the waveforms in this case.

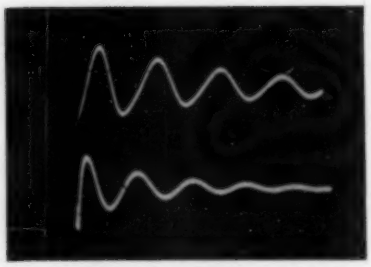


Fig. 6. Compare these normal "ringing" waveforms with those in Fig. 5.

It's evident from the wave configurations in Fig. 5 that there are shorted turns in the old transformer's primary, secondary, or both. The effect was insignificant with the transformer cold, but continued operation of the receiver made the condition steadily worse until the circuit eventually resonated at 120 cycles instead of 60 . . . a real mystery to an ohmmeter, but a "natural" for an oscilloscope.

After a few finishing touches, mostly in the sync circuits, the set was ready for Joe to pick up and take home. In spite of my forebodings, the job had not been so bad after all, and this particular 21F1 is now in good enough condition that I don't expect to see it again for some time. ▲

Regeneration

(Continued from page 29)

cently brought in with the complaint that the raster broke up into coarse horizontal lines through which no picture detail could be seen. The set acted normally when turned on. Assuming that I was dealing with a severe and intermittent horizontal-frequency trouble, I let the receiver operate for some time; but the symptom still did not appear. Finally, I removed the rear cover, and attached a cheater cord. In so doing, I disconnected the antenna, thereby bringing forth the ragged-line symptom shown in Fig. 1B. Since the chassis type and complaint were the same as in the previous case, I half-hoped the trouble source would prove to be the same. Sad to relate, the cause was different.

Trying all the tricks known to cure oscillation led nowhere. As is usual in such cases, an accidental discovery finally pointed to the solution. I found the trouble could be made to disappear if the shield enclosing the first IF transformer was pushed in a certain direction. An examination of all the grounding lances on this shield revealed that one was not soldered to the printed board. One drop of solder, and the trouble was gone.

I have found this same condition in five of these chassis thus far, with the cause and cure always the same. The shield, shown in Fig. 4 as an oblong object marked with an X, is positioned at the top center of the vertically-mounted PW board. It has six separate grounding lances; the troublemaker is the one nearest the 6AQ5 socket.

Tube Pin Not Contacting Socket

Regeneration was observed in a new 1960-model Motorola portable when the set was removed from the factory-sealed carton for pre-delivery testing. Knowing that regeneration troubles can be time-consuming, we debated whether to work on the set or to return it to the distributor. We decided that we would at least remove the back and examine the chassis. This inspection revealed that the first IF tube was inserted at an angle. We seated the tube correctly in its socket, and — no more regeneration. Judging from the position of the tube, it appears that the suppressor grid was not contacting its socket connection. Ah, if only more jobs could be this simple!

Above Ground—Above 100 mc

We once took in a Muntz 624 which presented the breakup symptom only on Channel 10. The other available channels (3 and 6) operated normally, so this was obviously a case of tuner trouble. We therefore proceeded to examine the tuner wiring, which was accessible after removing all the turret strips except those for Channel 10. Gently probing the wiring, we spotted a broken solder connection to ground from pin 2 of the 3BC5 RF tube. Resoldering this connection provided a cure. Reference to a tube manual supplied the interesting information that pins 2 and 7 are internally connected in a 3BC5 tube. This means that pin 2, even with no external connection, was still grounded through pin 7. The internal connecting lead, less than ¼" long,

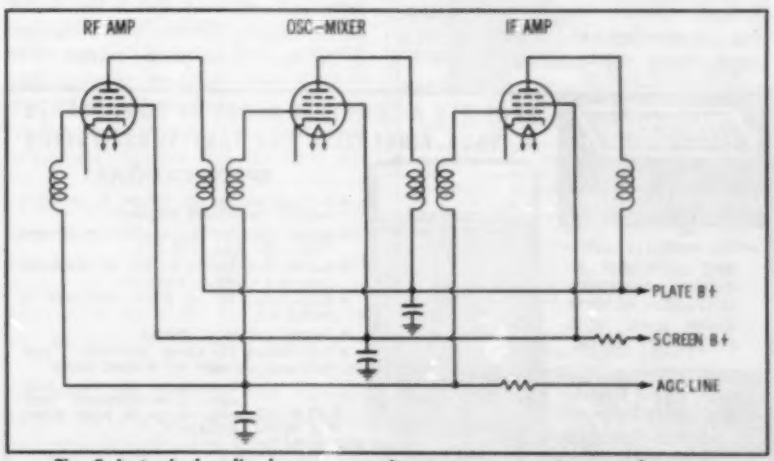
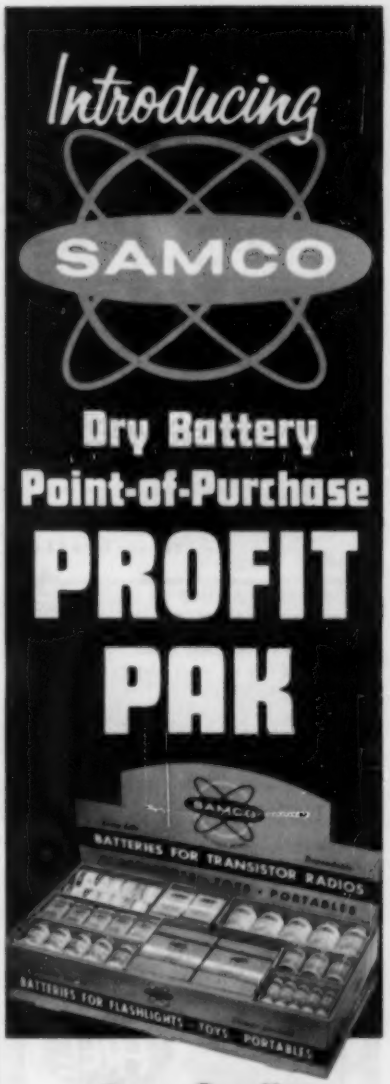


Fig. 5. In typical radio, bypass capacitors are common to several stages.



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provided enough inductance to create regeneration on the high-VHF band without affecting the lower frequencies.

Alignment

. . . or more appropriately, misalignment — does not produce such a large number of regeneration cases as might be expected. Tuned IF circuits seem to tolerate a wide latitude of misadjustment before regeneration or oscillation sets in, except when two adjacent stages are peaked at the same frequency. Oscillation is then much more easily induced by improper alignment.

We once unearthed this condition in a Bendix T-19 which we were servicing for sync trouble. The poor sync was directly attributable to a shorted capacitor and a charred, off-value resistor. After replacing these, we could lock in a picture, but oh, what a picture! It had no clear definition, and was rich in multiple images. When we tried the "no antenna" test, raster breakup appeared, so we knew we were again face-to-face with our old f(r)iend, regeneration. Suspecting that the IF slugs had been fiddled with by the owner or his brother-in-law, we fired up the sweep generator and attached the scope. Honestly, the bandpass waveform was so jagged that I doubt it could be equaled *intentionally*. Happily, the bandpass responded to realignment, and we were able to return the set with good picture and sound.

Lead Dress

Regeneration due to poor lead dress is most often the result of previous servicing, during which certain critically-positioned wiring was unknowingly re-routed. For example, take the case of an RCA Chassis KCS47 which presented typical symptoms of regeneration. In the shop, the usual cures were applied without success. Finally, it was noticed that the shielded cable feeding audio to the volume control was running almost parallel to the entire IF strip. Shifting the cable to its orthodox position along the end apron of the chassis cleared up the regeneration.

Disturbed lead dress can also cause the decline in picture quality and sync stability frequently noted in Muntz 624 receivers. Improvement calls for a careful repositioning of the leads in the last IF transformer. It is not possible to describe the operation as "shift red lead ⅛" forward," etc., but directions can be given as follows: Operate the set without an antenna and check for raster breakup. If breakup occurs, remove the shield covering the wiring beneath the second IF tube (a 6BA8); in doing so, look for evidence of the shield having been previously removed. Check the value of the bias resistor on the cathode of the 6BA8 pentode; it should be 100 ohms. Now, with the set on and regeneration present, separate and dress the leads of the transformer until the regeneration symptoms disappear from the raster. (Of course, a fiber or plastic dressing tool must be used in order to avoid detuning the circuit.) Now try the set on a station with normal antenna; a definite improvement in both picture and sync will very probably be revealed.

If further improvement in picture quality is sought, carefully tune the fine-tuning control for the best possible picture; then watch the screen while making further slight changes in the lead dress of the transformer.

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This lead-dress problem has been uncovered in several receivers of this same model. In each case, the orginal cause of the trouble appears to have been a heater-to-cathode short in the 6BA8 tube, leading to a burnout or change in value of the cathode resistor. Whenever this resistor is replaced, it is highly probable that the unsuspecting serviceman will accidentally move the transformer leads to incorrect positions.

Defective Decoupling—Common Cause?

TV servicemen who got their start in radio servicing are naturally inclined to troubleshoot regeneration in TV receivers by the same method they successfully employed to locate the cause of motorboating or chirping in radios. Most frequently the result is only a waste of time. Despite the fact that RF-IF regeneration produces comparable results in both radios and TV's, the actual cause is very often not the same.

In radios, regeneration is due to defective decoupling networks approximately 90% of the time. The balance of the problems are caused by poor shielding, tubes, lead dress, etc. On the other hand, regeneration in TV receivers is due to defective decoupling networks in only about 10% (or less) of all cases, and then only in receivers of simplified design. A comparison of RF-IF signal circuits in radio and TV receivers will immediately reveal why this is so. Fig. 5 is a typical circuit of the RF-IF portion of a radio, with emphasis placed on the decoupling networks; Fig. 6 is a schematic of the corresponding sections in a typical TV receiver. Note that the screen grids of all the various stages in the radio are tied together and bypassed with a single capacitor. The same is true of the plate and grid circuits. In Fig. 6, however, note that each individual element has its own RF bypass capacitor and series resistor to decouple it from the other feed lines in the B+ and AGC circuits. (In some receivers, the plate and screen of a stage share a common decoupling network, but isolation is still maintained between stages.)

Therefore, if an RF bypass on the common line feeding the various screen grids in the radio circuit were to open, regeneration or oscillation would almost certainly occur as a

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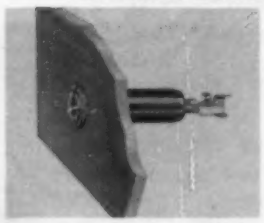
PRODUCT report

For further information on any of the following items, circle the associated number on the Catalog & Literature Card.

Tube-Transistor Handbook (41W)

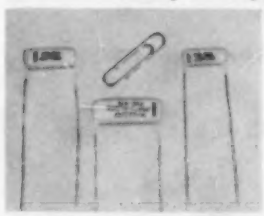
A revised 1960 edition of the **CBS** "Technician's Handbook" has just been issued. This 480-page, 5" x 9" book provides technical data for receiving, industrial, hi-fi, special-purpose, and foreign tubes; an expanded transistor and crystal-diode section; a complete picture-tube data chart; and a transistor cross-reference chart. The comb binding permits the book to lie open at any page. Price is $1.95.

Jack for Thick-Panel Mounting (42W)



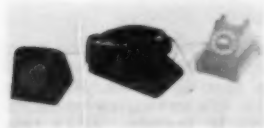
Equipped with an extra-long threaded barrel, the **Switchcraft** "Thick Panel Phone Jack" lends itself to mounting in a panel or wall up to 1¼" thick. This style of jack is designed to accept standard "Littel Plugs." Two types are available—two-conductor (Part No. 151) at a list price of $1.35, and three-conductor (No. 152B) at $1.50.

Mylar Capacitors (43W)



The light-blue outer coating of **Mallory PVC** capacitors is made of flexible polyvinyl chloride that allows the leads to be bent freely in any direction without risk of cracking the moistureproof seal. This material is also unaffected by heat applied during soldering. Units rated at 600 VDC are available in 42 values ranging from .001 to .47 mfd; there are also three other series, respectively rated at 400, 200, and 100 VDC. Capacitance tolerance of all types is ±10%.

Telephone Accessory (44W)



The **RMS** Model TA-4 "Ampli-Phone" allows the user to carry on phone conversations without holding the instrument to his ear. When the telephone receiver is placed on the unit's cradle, incoming voices are amplified and fed to a movable 4" speaker. (Output volume is adjustable.) For transmission in the other direction, a parabolic pickup device focuses room sounds on the telephone mouthpiece, effectively amplifying the outgoing portion of the conversation. Power requirement of the TA-4 is 110 to 120V, AC or DC; retail price is $39.95.

Semiconductor Specialties (45W)

Several new series of semiconductor devices have been introduced by **Sarkes Tarzian.** High-voltage silicon cartridge rectifiers are available as ferrule-mounted or axial-lead units; PIV ratings of various types range from 1,000 to 16,000 volts. Silicon Zener voltage-regulator diodes are supplied in ratings from 5.6 to 100 volts at ¼, 1, or 10 watts. A number of modular silicon rectifiers are also available for use as open bridges or for easy assembly into various 3- or 6-phase configurations.

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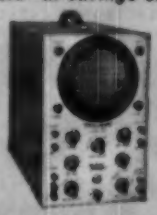

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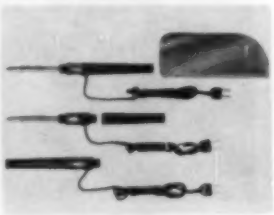
Pocket-Size Soldering Iron (47W)

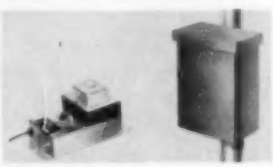


The "Solder-Chief" Model A-1000 pencil iron, manufactured by **L. I. Electro-Labs,** has a removable hollow handle which can be utilized as a sheath for the soldering tip — permitting the iron to be transported safely while still hot. Length is 10½" in use, 6½" when closed; weight is 13 oz.; power rating is 30 watts.

Ceramic Microphone (48W)

An omnidirectional, high-impedance ceramic microphone for audio-visual labs, PA systems, and communication stations, the **Sonotone** Model CM-17 "Flex-Mike" has a rubber-cushioned transducer mount for increased shock resistance. The flexible 13" stand terminates in a removable mounting plate. Sensitivity is –56 db, and frequency response is 50 to 13,000 cps with a controlled amount of midrange boost for added "presence." Price is $24.50.

Mast-Mounted VHF Preamp (49W)



The two-tube **Jerrold** Model DSA-202 "De-Snower" preamplifier provides 20-db gain on all VHF-TV channels, with a maximum noise figure of 4.5 db on the low band and 6 db on the high band. An improved type of remote power supply includes a switch to adjust the amplifier-supply voltage according to cable length. A sliding cover on the 8½" x 6¼" x 4" case gives access to the tubes. List price is $79.95.

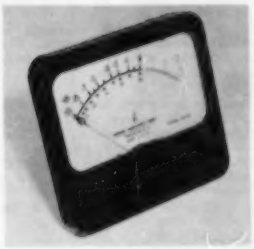
AC-DC Radio Tubes (50W)

Some of the newest AC-DC radio receivers are using tubes with a 100-ma heater current (instead of the conventional 150 ma) for the purpose of reducing heat dissipation. **RCA** has announced a series of five tubes for this service, including the 18FX6 pentagrid converter, 18FW6 IF pentode, 18FY6 twin diode/high-mu triode, 34GD5 beam-power output tube, and 36AM3A rectifier. A different series, for low-cost four-tube radios, comprises the 36AM3A, 18FX6, 20EQ7 detector diode/IF pentode, and 50FK5 high-sensitivity power-output tube. The audio and rectifier tubes in these groups are also applicable to inexpensive stereo phonograph circuits.

Wire-Wound Resistors (51W)

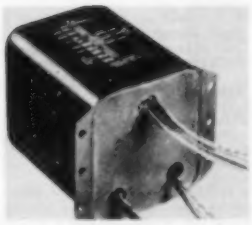
Six different wattage sizes of **IRC** Type PW resistors are available—3, 5, 7, 10, 15, and 20 watts. The wire element is wound on a glass fiber core and sealed in a rectangular ceramic case filled with a fireproof, inorganic material. Ranges of values available are as follows: For 3 and 5 watts, 0.1 to 7500 ohms; for 7 watts, 0.1 to 18K ohms; for 10 and 15 watts, 0.18 to 30K ohms; and for 20 watts, 0.6 to 5100 ohms. Both 5% and 10% tolerances are furnished.

VU Meter (52W)



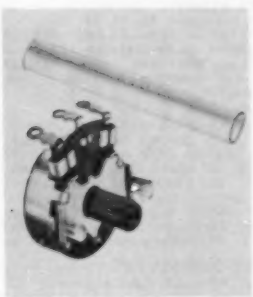
A VU meter for precise indication of recording level in tape recorders, the **Robins** Model VU-100, has both low- and high-impedance inputs. A 200-ua meter movement produces readings on a 2-color scale covering a range from –20 to +3 VU; in addition, there is a 0-100% modulation scale. The unit is 1½" deep and mounts in a 2¾"-diameter hole; its list price is $22.

Audio Transformers (53W)



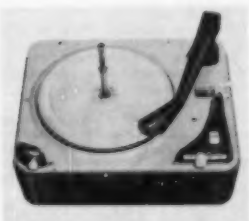
Chicago Standard Transformer Corp. has announced a 65-watt high-fidelity audio output transformer, the BO-15, intended for use with 6550, EL34, or KT88 tubes in a 40- or 60-watt amplifier having tertiary feedback. Complete construction details for these amplifiers are available on request. Also newly introduced are three new PA transformers for matching 8- and 16-ohm speaker voice coils to a 70.7-volt line. Model numbers and power ranges are as follows: A-8080, 1-5 watts; A-8081, 6-10 watts; and A-8082, 11-15 watts.

Switches and Controls (54W)



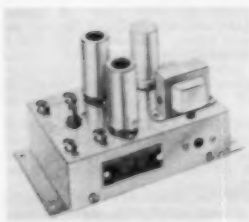
Centralab Model TT controls have very short, slotted shafts, and a 2" polyethylene tube is packed with each control for use as a shaft extension where needed. These half-watt, twist-tab units come in 25 values from 200 ohms to 7.5 megohms. Other new products include a complete line of push-pull and push-push on-off switches in universal - shaft, "Adashaft," "Fastatch," and stereo-twin types, plus a No. 1486 "Local - Remote - Both" stereo speaker switch.

Stereo Changer (55W)



The **EICO** "Dual-1007" can operate as a changer accommodating up to 10 records, or as an automatic or manual single-record player. Included with the unit is a snap-in stereo crystal cartridge with dual styli —0.7 mil diamond and 3-mil sapphire in Model 1007D ($59.75), or 0.7- and 3-mil sapphires in Model 1007S ($49.75). Accessories include metal base MB-1 at $3.95, automatic 45-rpm spindle 45AS at $4.80, and precut wood mounting board WM-1 at $2.40.

Phono Preamp (56W)



The **Shure** Model M65 preamplifier provides the added small-signal amplification and equalization needed to operate a magnetic cartridge with an amplifier originally designed for a ceramic cartridge (for example, most of those included in packaged stereo phonographs). The only restriction is that the changer used with the preamp must have a 4-pole motor to avoid excessive hum. The M65, which can also be employed as a tape or mike preamp, is priced at $24.

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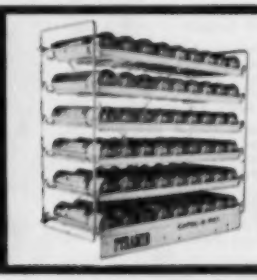

JEWEL BOX

Handsome tan plastic, high impact cabinet with 9 drawers, contains 45 assorted Mylar*-paper Gold Dip capacitors, type 151. Practical . . . convenient . . . for storage in your shop, or home. Actual value of the Jewel Box with 45 Gold Dip capacitors—$19.50, dealer net only $9.25.

Gold Dip capacitors are also available in Clear-Vu paks . . . 5 to a package. Find them on Pyramid's new Whirl-o-mat on your favorite parts distributor counter.

"GOLD STANDARD" 111 KIT
Clear lucite hinged box containing 75 Pyramid's popular assorted Gold Standard Mylar* capacitors. You'll find so many uses for the Gold Standard 111 Kit. Actual value is $26.00, dealer net only $13.00.

515 LYTIK-KIT
Hinged cover, clear lucite box with 15 assorted miniature low voltage electrolytic capacitors for transistorized circuit replacements, type MLV. This Kit is a constant companion to any busy serviceman. Actual value, $20.60, dealer net only $10.30.

PYRAMID ELECTRIC COMPANY
DISTRIBUTOR DIVISION: UNION CITY, NEW JERSEY
Factories: Gastonia, North Carolina • Darlington, South Carolina
In Canada: Wm. Cohen, Limited, 8900 Tanguay Street, Montreal
Export: Morhan Exporting Co., 485 Broadway, New York 13, N.Y.

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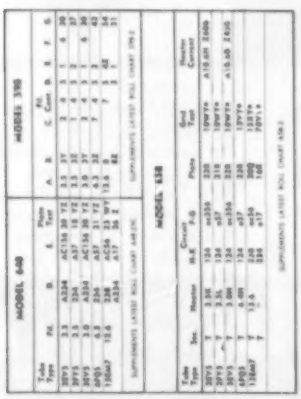


CATALOG AND LITERATURE SERVICE

ANTENNAS AND ACCESSORIES

1W. FINNEY — Large *Performance Guide* wall chart describing complete line of *Field-Proven* TV and FM antennas, specifying performance of each FINCO antenna as determined through use of the *Mobile Research Laboratory Unit*.

2W. JFD—1960 Exact-Replacement Antenna Guide for Portable and Toteable TV sets (20 pages), compiled and edited by Howard W. Sams & Co., Inc. Gives TV receiver model number, manufacturer's antenna part number, and model number of corresponding JFD exact-replacement antenna. Also Form 940 dealer catalog illustrating and describing 1960 line of natural silver and gold anodized *Hi-Fi* TV antennas, mounts, masts, and accessories. *See ad page 21.*

3W. MOSLEY—Catalog of TV antenna and audio accessories; also sample mailing piece designed to help service dealers promote Model F-1PK TV Wall Outlets. *See ad page 36.*

4W. WINEGARD—Descriptive catalog with schematic drawing on 1- to 30-set distribution amplifier Model A-400. *See ad page 34.*

AUDIO & HI-FI

5W. CBS ELECTRONICS—Retail price list and cross-reference chart of *CBS-Ronette* phono cartridges. *See ad page 43.*

6W. DUOTONE — "How-to-" booklet on identifying and replacing phono needles; wall chart of replacement-needle data; needle identification and replacement catalog to bona fide dealers and repairmen. *See ad page 62.*

7W. EICO—New 28-page 1960 catalog of kits and wired equipment for stereo and monophonic hi-fi, test instruments, "ham" gear, Citizens band transceivers, and transistor radios. Also "Stereo Hi-Fi Guide" and "Short Course for Novice License." *See ad page 69.*

8W. SWITCHCRAFT — New-product bulletins on *Thick Panel Phone Jack* for mounting in any panel up to 1¼" thick, and on TR Series *Micro-Plugs* which match ultra-miniaturized *Micro-Jax*.

COMPONENTS

9W. BUSSMANN—Three-color bulletin on two types of *Stak-Pak* fuse assortments, showing TV servicemen how new packaging idea provides convenient way to carry a complete line of fuses at all times. *See ad page 37.*

10W. CHICAGO STANDARD—Form P-60-P, short-form *TV Replacement Guide*. *See ad page 53.*

11W. EASTERN JEWEL—Catalog 160 describing exact replacement line of printed-circuit electrolytics, and non-polarized types for hi-fi crossover networks; miniature "buzz" controls; ferrite rod antennas; push-push switches; frozen yoke remover. *See ad page 58.*

12W. PYRAMID — New "hang-up" Catalog J-10 on expanded line of replacement capacitors. *See ad page 71.*

13W. SPRAGUE—44-page Catalog C-613a, describing all popular replacement components in company's line. *See ad page 10.*

14W. SAMPSON — *Transistor Battery Data and Reference Guide*, with size, price, and cross-reference data on batteries used in Japanese transistor radios; also information on "Point-of-Purchase Profit Pak," a counter display for *Samco* dry batteries. *See ads pages 64, 65.*

15W. WORKMAN—Catalog sheet describing non-inductive dummy load resistors available in ratings from 10 through 500 watts for service-shop and industrial applications, and for special functions such as parasitic suppression.

PROMOTIONAL AIDS

16W. SYLVANIA — Free booklet No. 2015, "*. . . And Now a Word From Sylvania*," telling dealers how to tie in with national advertising campaign featuring the most successful salesman in the U.S.A. — Arthur Godfrey. *See ad page 9.*

RADIOS & PHONOGRAPHS

17W. ELECTRONIC PRODUCTS CORP.—Brochure and dealer price list on battery-operated, transistorized Futura portable phonographs, radios, and combinations.

SERVICE AIDS

18W. CASTLE—Leaflet describing fast overhauling service on television tuners of all makes and models. *See ad page 51.*

19W. CHEMICAL ELECTRONICS — Descriptive folder on *HUSH, EVER QUIET, EVER KLEER*, and *SURE-N-EASY* electronic chemicals. *See ad page 40.*

20W. PRECISION TV TUNER — Information on repair and alignment service available for any type of TV tuner. *See ad page 62.*

21W. SWING-O-LITE—Literature on *Inspector* swiveling bench lamp with fluorescent bulb and built-in magnifying lens, and on *Craftsman* shaded bench lamps in choice of goose-neck and swinging-arm styles.

22W. VIDAIRE—Comprehensive catalogs of TV-radio accessories, service aids, and hi-fi accessories; also cross-reference sheet on power transistors.

SPECIAL EQUIPMENT

23W. ATR—Data on complete line of emergency lighting and power supply units for use in the event of commercial power-line failure. *See ad page 16.*

24W. RADIO MERCHANDISE SALES (RMS) — Information on Model TA-4 *Ampli-Phone* which enables user to carry on telephone conversations while phone receiver rests on desk or table.

TECHNICAL PUBLICATIONS

25W. GENERAL ELECTRIC—10-page guide to profitable servicing, *Techni-Talk*, with work-saving short cuts, and photographic reproductions of TV faults. *See ad page 35.*

26W. J. W. MILLER—Vol. 1, Nos. 1 and 2 of *The Coil Forum*, a new technical bulletin to assist electronics experimenters in designing and constructing equipment, featuring hints on wise use of coils. Also data sheet on *J-Trap* miniature IF transformers. *See ad page 20.*

27W. MOTOROLA—Complete brochure describing Motorola Institute training course on two-way radio communications, plus sample lesson SA-7 on transistorized receiver circuits.

28W. RCA INSTITUTES — 64-page illustrated booklet describing comprehensive training program for home study, ranging from electronics fundamentals to transistors and automation. *See ad page 32.*

29W. RIDER—Latest book list. *See ad page 40.*

30W. HOWARD W. SAMS—Literature describing all current publications on radio, TV, communications, audio and hi-fi, and industrial electronics servicing. *See ads pages 50, 54, 55, 66.*

31W. SYLVANIA HOME ELECTRONICS—Information on availability of service literature on television, radio and high fidelity, and monthly *Service Digest*. *See ad page 44.*

TEST EQUIPMENT

32W. B & K—Bulletin AP16-R gives information on new Model 1076 *Television Analyst*, Models 1070 and A107 *Dyna-Sweep Circuit Analyzers*, Models 550, 650, 675, and new 685 *Dyna-Quik* dynamic mutual conductance tube testers, new Model 160 Transistor Tester, and Model 440 CRT rejuvenator-tester. *See ad page 47.*

33W. ELECTRO PRODUCTS — Information on Model PS-3 low-cost regulated DC power supply for servicing transistor circuits. *See ad page 63.*

34W. MERCURY—Bulletin 103, giving complete specifications on new Model 103 tube tester plus full information on other instruments in the line. *See ads pages 50, 62, 66, 68.*

35W. SENCORE—New booklet, *How to Use the SS105 Sweep Circuit Troubleshooter*, plus brochure on complete line of *time-saver* instruments. *See ads pages 12-13, 14-15.*

TOOLS

36W. BERNS—Data on 3-in-1 picture-tube repair tool, on *Audio Pin-Plug Crimper* that lets you make pin-plug and ground connections for shielded cable without soldering, and on *ION* adjustable beam bender. *See ad page 67.*

37W. L. I. ELECTRO-LABS — Flyer on *Solder-Chief* Model A-1000 *Solder-Pen*, a 30-watt pencil-type iron with removable handle which fits over the tip so the iron can be carried around while still hot.

TUBES AND TRANSISTORS

38W. AMPEREX — New 25-page condensed catalog containing descriptions and specifications on full line of tubes. Covers cold cathode trigger types, entertainment tubes, ignitrons and thyratrons, magnetrons, klystrons, noise diodes, power tubes, photomultiplier tubes, radiation counter tubes, traveling wave and UHF special tubes. *See ad page 41.*

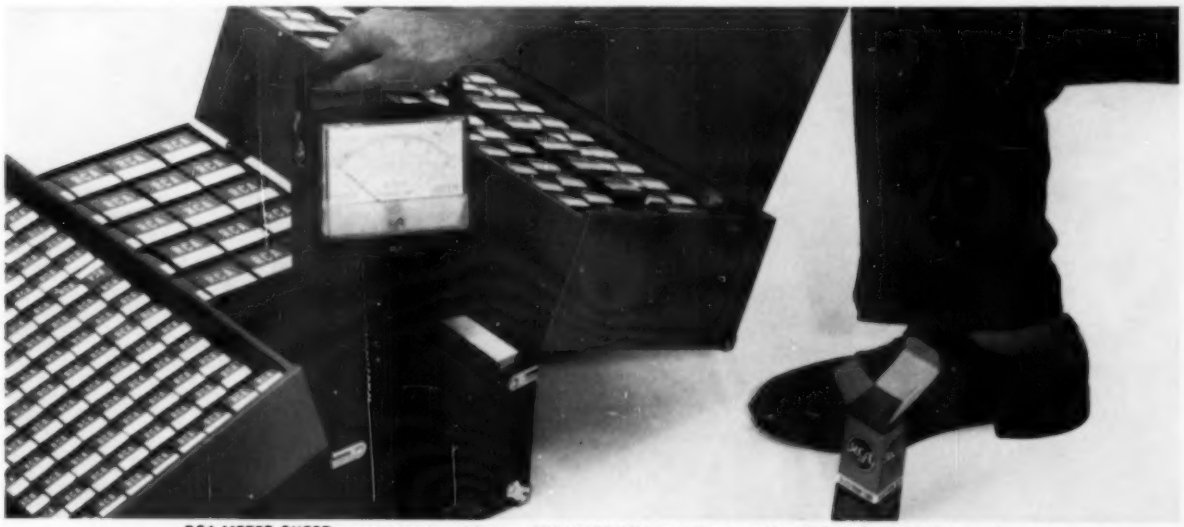
39W. ELECTRONIC TRANSISTOR CORP.—Transistor interchangeability chart—recommended replacements from American-made ETCO *J800 Series* for Japanese types.

40W. SAMPSON — *Hitachi* receiving-tube manual, giving extensive specifications, basing diagrams, and outlines for complete tube line; also catalog sheet with color photos and descriptions of *Hitachi* broadcast-band and two-band transistor radios. *See ads pages 64, 65.*

RCA FRONT PAGE NEWS

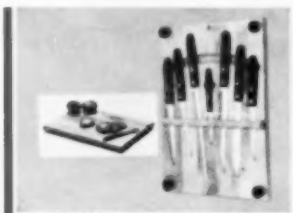
NOW FOR A LIMITED TIME, GET VALUABLE SERVICE AIDS AND GIFTS WHEN YOU BUY RCA TUBES!

RIGHT NOW's the best time to stock up on the RCA receiving tubes you'll need through the coming season. Shown here are *just a few* of the exciting gifts and premiums you get FREE with RCA tubes purchased from participating RCA distributors.



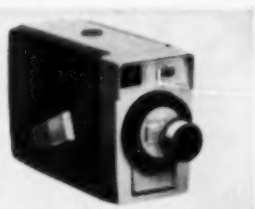
RCA METER-CHEST—a combination of famous RCA WV-38 VOM and "Treasure Chest" Tube Caddy. 750 tubes!*

TV TOTER TABLE—simplifies moving heavy chassis. 350 tubes.*

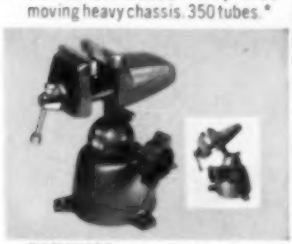


CUTLERY SET—7 utensils and cutting board. 325 tubes.*

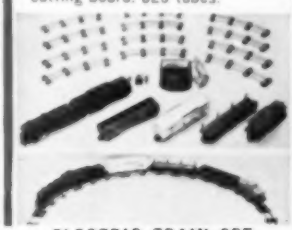
KODAK BROWNIE PHOTO OUTFIT—550 tubes.*



BROWNIE 8 MOVIE CAMERA—575 tubes.*



PANAVISE—for easier bench work. 300 tubes.*



ELECTRIC TRAIN SET—350 tubes.*

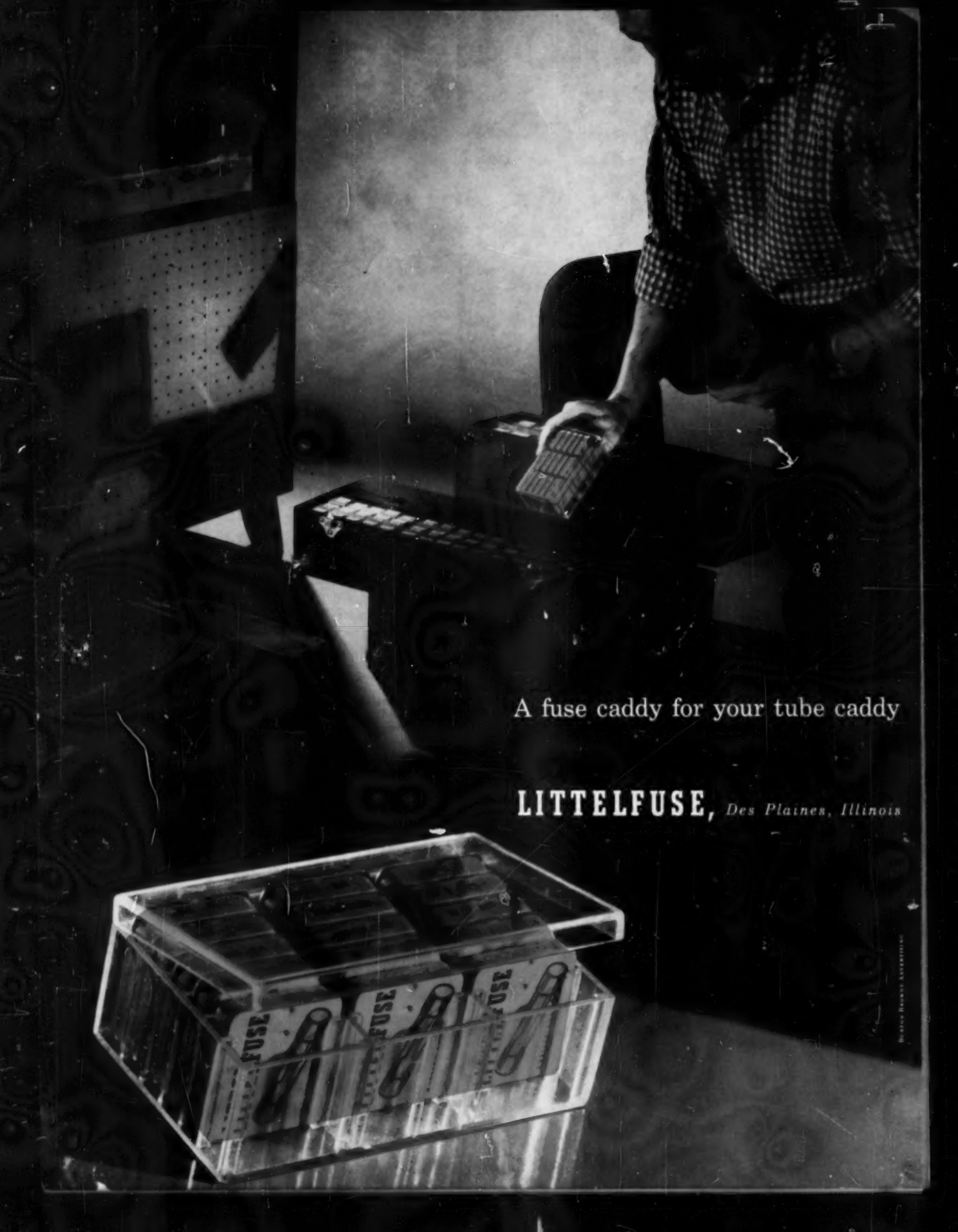
MAN'S WATCH—precision swiss movement. 475 tubes.*

LADY'S WATCH—precision swiss movement. 475 tubes.*

For complete selection of gifts and full details, check with your participating RCA distributor.

Suggested Value

The Most Trusted Name in Electronics
RADIO CORPORATION OF AMERICA


A fuse caddy for your tube caddy
LITTELFUSE, Des Plaines, Illinois
FUSE
FUSE
FUSE